

$$\sum M_A = 0 = V_B \cdot 5m - 10kN(4m + 2m + 3m + 4m) \rightarrow V_B = 26kN$$

$$V_A + V_B = 30kN \rightarrow V_A = 4kN$$

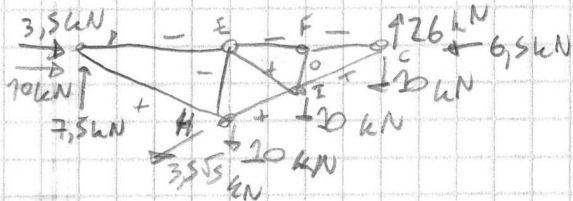
$$\sum M_C^{der} = 0 = H_B \cdot 4m - V_B \cdot 7m \rightarrow H_B = 6,5kN$$

$$H_A + H_B = 10kN \rightarrow H_A = 3,5kN$$

$$\sum M_D = 0 = F_{GH} \cdot \frac{2}{\sqrt{5}} \cdot 2m - 3,5kN \cdot 4m \rightarrow F_{GH} = 3,5\sqrt{5}$$

$$\sum F_H = 0 = H_D + 3,5kN - 3,5\sqrt{5} \cdot \frac{2}{\sqrt{5}} \rightarrow H_D = 3,5kN$$

$$\sum F_V = 0 \rightarrow V_D = 4kN + 3,5\sqrt{5} \cdot \frac{1}{\sqrt{5}} = 7,5kN$$



Node D: $F_{DE} = 7,5kN$, $F_{DH} = 7,5\sqrt{5}kN$

$$F_{DE} = 7,5kN + 7,5\sqrt{5} \cdot \frac{2}{\sqrt{5}} = 28,5kN$$

Node H: $F_{HI} = 7,5\sqrt{5}$, $F_{EH} = 3,5\sqrt{5}$

$$F_{HI} \cdot \frac{2}{\sqrt{5}} = 7,5\sqrt{5} \cdot \frac{2}{\sqrt{5}} + 3,5\sqrt{5} \cdot \frac{2}{\sqrt{5}} \rightarrow F_{HI} = 17\sqrt{5}kN$$

$$F_{EH} + 10kN + 3,5\sqrt{5} = 7,5\sqrt{5} \cdot \frac{1}{\sqrt{5}} + 17\sqrt{5} \cdot \frac{1}{\sqrt{5}} \rightarrow F_{EH} = 5kN$$

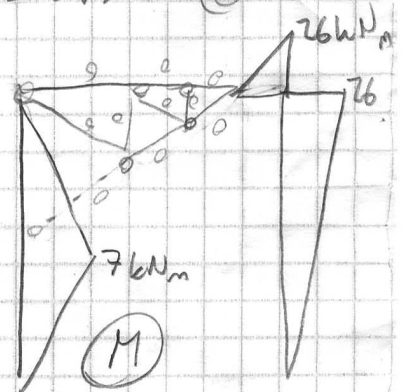
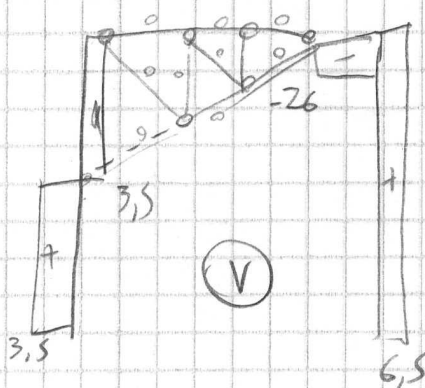
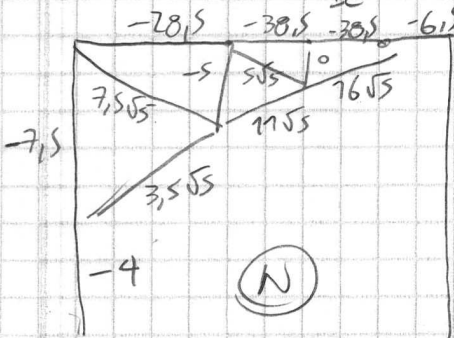
Node E: $F_{EF} = 5kN$, $F_{EI} = 28,5kN$

$$F_{EI} \cdot \frac{1}{\sqrt{5}} = 5kN \rightarrow F_{EI} = 5\sqrt{5}kN$$

$$F_{EF} = 28,5 + 5\sqrt{5} \cdot \frac{2}{\sqrt{5}} = 38,5kN$$

Node C: $F_{IC} = 38,5kN$, $F_{EC} = 16kN$

$$F_{IC} \cdot \frac{1}{\sqrt{5}} = 16kN \rightarrow F_{IC} = 16\sqrt{5}kN$$



- Mayor directa $-38kN$ $\sigma \geq \frac{38,5kN}{14kN/cm^2} \geq 1,66cm$

- $M = 26kNm$ $N = 26kN$ Aproximo $W \geq \frac{2600kNm}{14kN/cm^2} = 185,7cm^3$

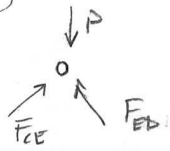
PNI 20 tiene $W = 274cm^3$ y $A = 33,5cm^2$

Verifico $\sigma = \frac{2600kNm}{274cm^3} + \frac{26kN}{33,5cm^2} = 12,7 \frac{kN}{cm^2} + 0,78 \frac{kN}{cm^2} < 14 \frac{kN}{cm^2}$

PNI 20 para barras con M y N.

EJ

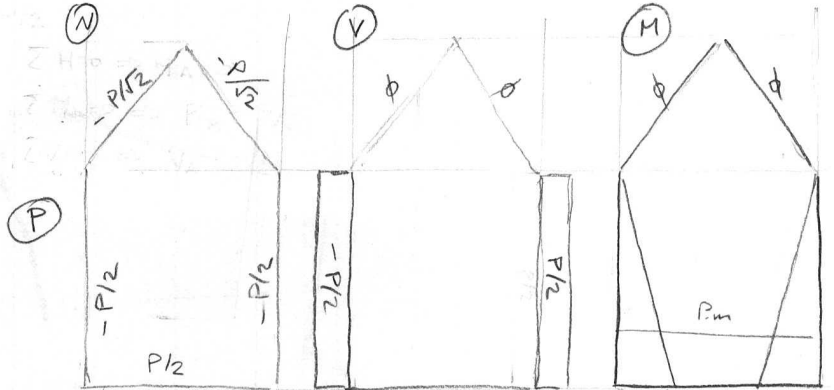
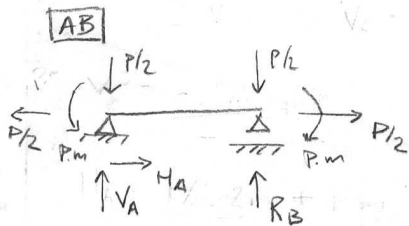
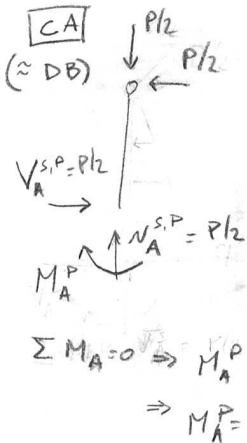
por P



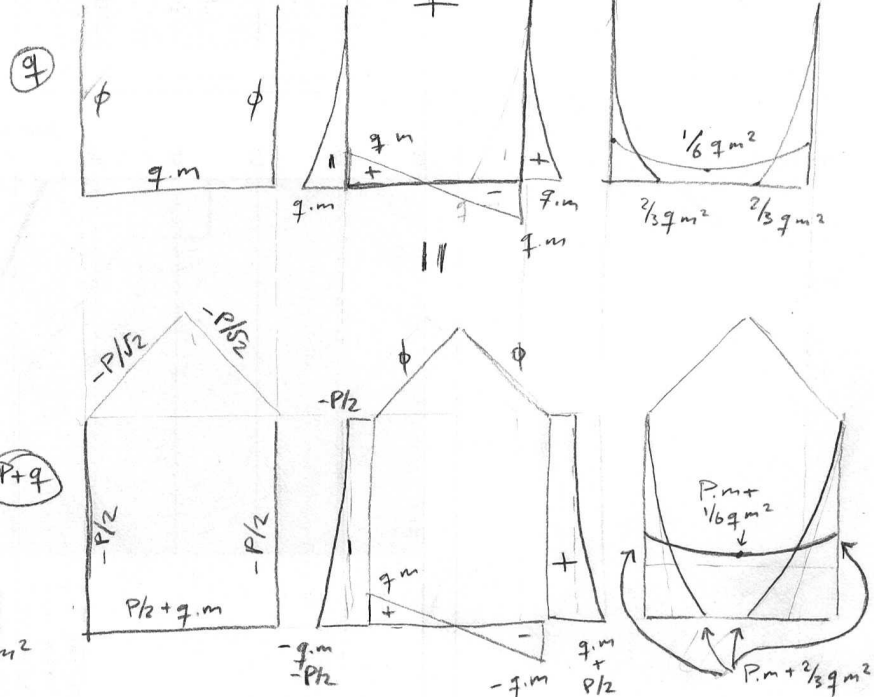
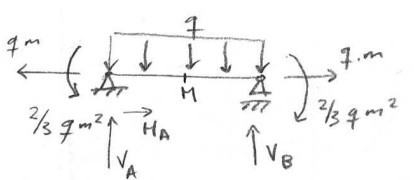
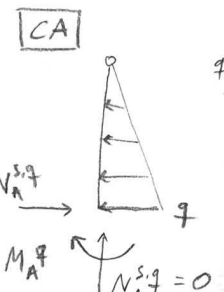
$$\sum H = 0 \Rightarrow F_{CE} = F_{ED}$$

$$\sum V = 0 \rightarrow \frac{F_{CE}}{\sqrt{2}} \cdot 2 = P \Rightarrow F_{CE} = P/\sqrt{2}$$

CE y ED bielas (solo directas)

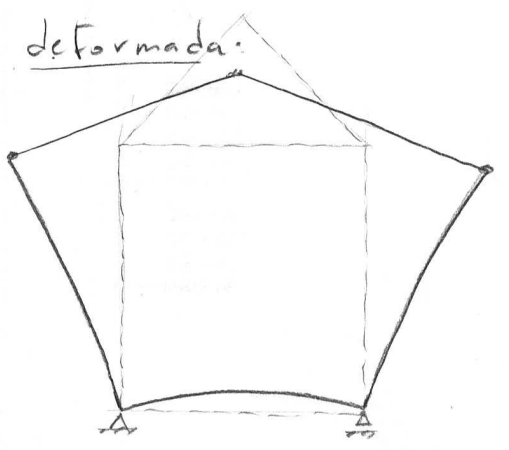


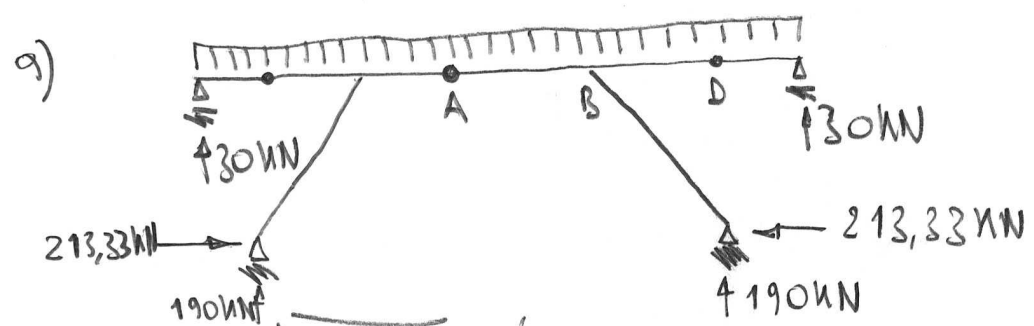
por q CE y ED inactivas



b) $100 \text{ MPa} = \frac{q \cdot m}{33,5 \text{ cm}^2} + \frac{2}{3} \frac{q \cdot m^2}{214 \text{ cm}^3} \Rightarrow 10 \frac{\text{KN}}{\text{cm}^2} = q \cdot m \left(\frac{1}{33,5 \text{ cm}^2} + \frac{200}{3 \cdot 214 \text{ cm}^3} \right) \Rightarrow q_{adm} = 29,3 \text{ KN/m}$

c) $\theta_A^q(\psi) = \frac{2/3 q m^2 \cdot 2m}{2EI} - \frac{q \cdot (2m)^3}{24EI} = \frac{1}{3} \frac{q m^3}{EI}$
 $\int_c^f(\psi) = \frac{q \cdot (2m)^4}{30EI} + \frac{1}{3} \frac{q m^3}{EI} \cdot 2m = 1,2 \frac{q m^4}{EI}$
 $\theta_A^P(\psi) = \frac{P \cdot m \cdot 2m}{2EI} = \frac{P \cdot m^2}{EI}$
 $\int_c^P(\psi) = \frac{P/2 \cdot (2m)^3}{3EI} + \frac{P \cdot m^2}{EI} \cdot 2m = 3,33 \frac{P m^3}{EI}$
 $\int_c(\psi) = \frac{1,2 \cdot 29,3 \text{ KN/m} \cdot m^4}{4280 \text{ KN/m}^2} + \frac{3,33 P m^3}{4280 \text{ KN/m}^2} = 0,015 \text{ m}$
 $\Rightarrow P = \frac{(0,015 - 0,0082) \cdot 4280 \text{ KN}}{3,33 \text{ m}} \Rightarrow P = 8,72 \text{ KN}$

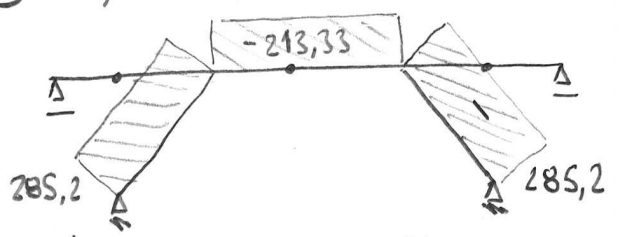




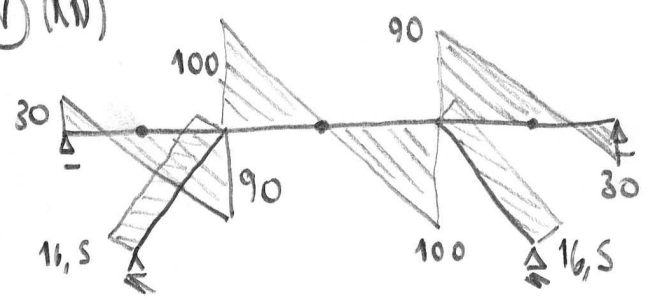
Aislo DE $\rightarrow N_E = 30 \text{ kN}$ / Eq global $\sum M_c = 0 \rightarrow 0 = 16V_c + 19 \times 30 \text{ kN} - 22 \times 20 \text{ kN} \times 8 - 30 \text{ kN} \times 3$
 $\hookrightarrow V_c = 190 \text{ kN}$

Eq en 1/2 estructura $\sum M_A = 0$
 $\hookrightarrow 20 \text{ kN} \times 11 \times 5,5 - 30 \text{ kN} \times 11 - 190 \text{ kN} \times 8 + H_c \times 3 = 0$
 $\hookrightarrow H_c = 213,33 \text{ kN}$

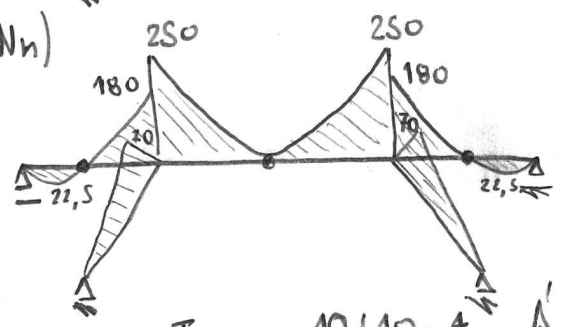
b) (N) (kN)



(V) (kN)



(M) (kNm)



c) PNI 36 $\rightarrow I_{x \text{ PNI}} = 19610 \text{ cm}^4$; $A' = 97,1 \text{ cm}^2$
 $I_{\text{tot}} = I_{\text{PNI}} + 2 \times [15 \times h \times (36/2 + h)^2 + 15 \times h^3 / 12]$; $y_{\text{sup}}^{\text{tot}} = 36/2 + h$
 $y_{\text{inf}}^{\text{tot}} = 36/2 - h$
 $\sigma_{\text{max}} = \frac{M \cdot y}{I_{\text{tot}}} + \frac{N}{A} \leq E \cdot \epsilon_{\text{max}}$
 $A'_{\text{tot}} = 97,1 + 2 \times 15 \times h$

-secciones a estudiar punto: - B por AB y fibra inferior (1)
 - B " BC y " " (2)

Tanteo $h = 10 \text{ mm}$

(1) $\sigma_{\text{max}} = 175,7 \leq 134 \times$
 (2) $\sigma_{\text{max}} = 66,9 \leq 134$

$h = 15 \text{ mm}$

(1) $\sigma_{\text{max}} = 152,5 \leq 134 \times$
 (2) $\sigma_{\text{max}} = 58,6 \leq 134$

$h = 20 \text{ mm}$

(1) $\sigma_{\text{max}} = 134,7 \leq 134 \times$
 (2) $\sigma_{\text{max}} = 52 \leq 134$

$h = 21 \text{ mm}$

(1) $\sigma_{\text{max}} = 131,6 \leq 134$ /
 (2) $\sigma_{\text{max}} = 50,9 \leq 134$

$\Rightarrow \boxed{h = 21 \text{ mm}}$