

Ejercicio 1

Parte A

- $\Sigma F_V = 0: V_A + V_F = 5 \frac{kN}{m} \cdot 4m + P$
- $\Sigma F_H = 0: H_A + H_F = 5 \frac{kN}{m} \cdot 4m$
- $M_C^{izq} = 0: 5 \frac{kN}{m} \cdot 4m \cdot 2m + H_A \cdot 6m = V_A \cdot 4m$
- $M_C^{der} = 0: 30kNm + P \cdot 2m + 5 \frac{kN}{m} \cdot 4m \cdot 3m = V_F \cdot 1m + H_F \cdot 6m$

Imponiendo que $V_A = 16kN$.

$$\begin{cases} V_F - P = 20kN - 16kN = 4kN \\ H_A + H_F = 20kN \\ H_A = \frac{16kN \cdot 4m - 40kNm}{6m} = 4kN \\ V_F + 6H_F - 2P = 30kN + 60kN \end{cases}$$

Entonces:

- $P = 10kN$
- $H_A = 4kN$
- $H_F = 16kN$
- $V_F = 14kN$

Parte B

Momento en B:

- $M_B = H_A \cdot 6m = 24kNm \cup$

El momento se anula en la barra BC en:

- $24kNm = \frac{16kN + (16kN - 5 \frac{kN}{m} x)}{2} x \Rightarrow x = 2,4m$

El momento antihorario máximo en BC es:

- $M = \frac{(0,8m)^2 \cdot 5 \frac{kN}{m}}{2} = 1,60kNm$

Cambio de solicitaciones en C:

- $N_C^{der} = \frac{N_C^{izq} \sqrt{2}}{2} + \frac{V_C^{izq} \sqrt{2}}{2} = \frac{-4kN \sqrt{2}}{2} + \frac{-4kN \sqrt{2}}{2} = -4\sqrt{2} kN = -5,66kN$
- $V_C^{der} = -\frac{N_C^{izq} \sqrt{2}}{2} + \frac{V_C^{izq} \sqrt{2}}{2} = \frac{4kN \sqrt{2}}{2} + \frac{-4kN \sqrt{2}}{2} = 0kN$

Solicitaciones en DE:

- $N_{DE} = -\frac{P \sqrt{2}}{2} = -7,07kN$
- $V_{DE} = -\frac{P \sqrt{2}}{2} = -7,07kN$

Momentos en nodo D:

- $M_D^{DE} = V_{DE} \cdot 1m \cdot \sqrt{2} = 10kNm \cup$

- $M_D^{CD} = 0 \text{ kNm}$
 $\Rightarrow M_D^{DF} = 10 \text{ kNm} \quad \cup$

Cambio de sollicitaciones en D:

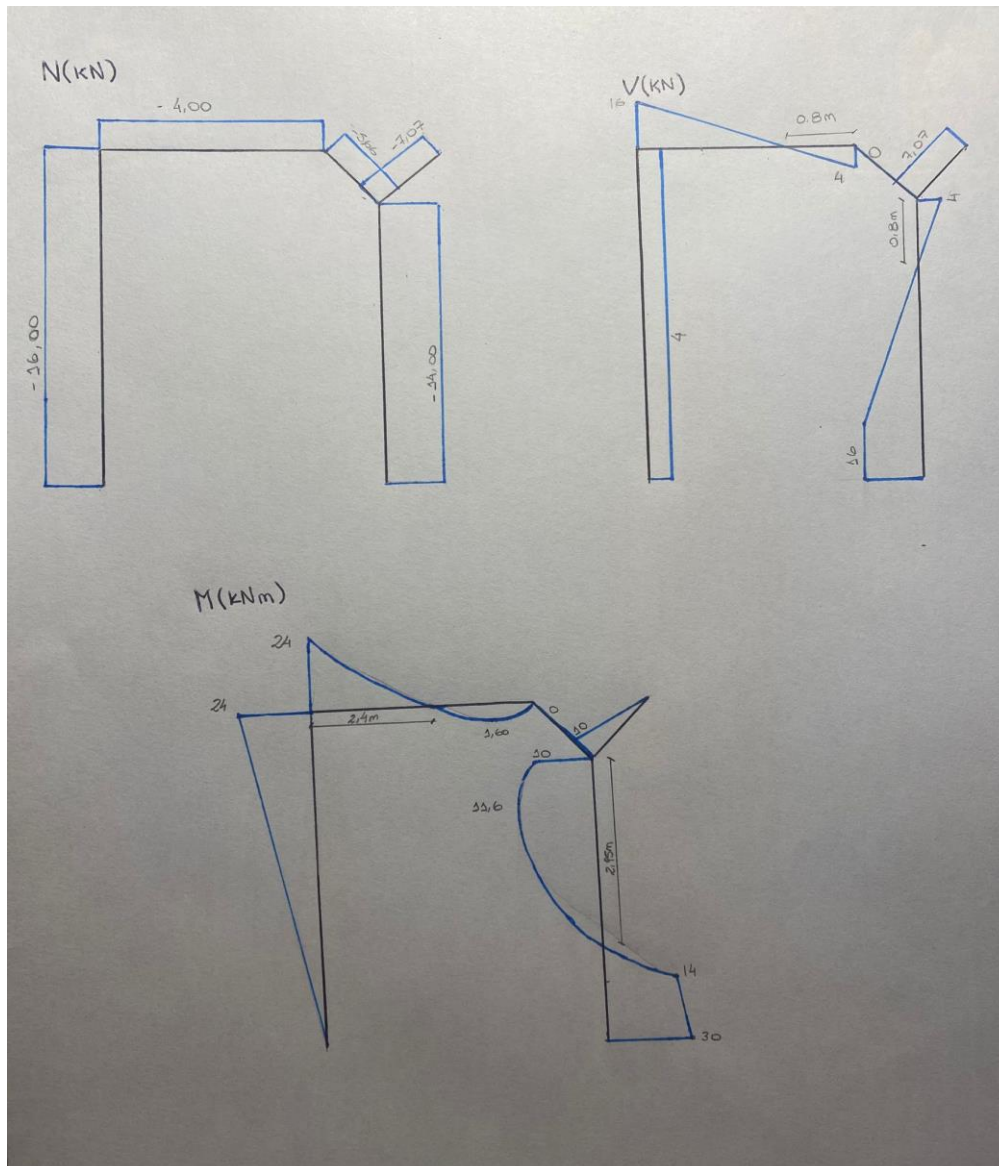
- $N_D^{DF} = \frac{N_D^{CD}\sqrt{2}}{2} + \frac{N_D^{DE}\sqrt{2}}{2} + \frac{V_D^{DE}\sqrt{2}}{2} = \frac{\sqrt{2}}{2}(-7,07 \text{ kN} - 7,07 \text{ kN} - 5,66 \text{ kN}) = -14 \text{ kN}$
- $V_D^{DF} = +\frac{N_D^{CD}\sqrt{2}}{2} - \frac{N_D^{DE}\sqrt{2}}{2} + \frac{V_D^{DE}\sqrt{2}}{2} = \frac{\sqrt{2}}{2}(-7,07 \text{ kN} + 7,07 \text{ kN} - 5,66 \text{ kN}) = -4 \text{ kN}$

Momento máximo antihorario en DF es:

- $M = 10 \text{ kNm} + \frac{(0,8 \text{ m})^2 \cdot 5 \frac{\text{kN}}{\text{m}}}{2} = 11,60 \text{ kNm}$

El momento se anula en DF en:

- $11,60 \text{ kNm} = \frac{5 \frac{\text{kN}}{\text{m}}(x-0,8 \text{ m})^2}{2} \Rightarrow x = 2,95 \text{ m}$



Parte C

Sección con cortante máximo

- 1) En la barra DF y BC, $V = 16kN$.

$$\tau = \frac{V\mu}{Ib} < \tau_{adm}$$

Secciones con mayor momento y directa:

- 2) En la barra AB con $M = 24kNm$ y $N = 16kN$.
3) En la barra DF con $M = 30kNm$ y $N = 14kN$.

$$\sigma = \frac{M}{W} + \frac{N}{A} < \sigma_{adm}$$

Pre dimensiono con $M_{max} = 30kNm$: $W > \frac{M_{max}}{\sigma_{adm}} = 214,3cm^3$

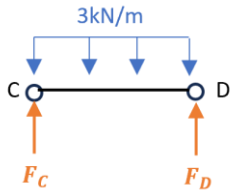
Tomo PNI 220: $W = 278cm^3$; $A = 39,5cm^2$; $I = 3060cm^4$; $\mu = 162cm^3$; $b = 8,1mm$

- 1) $\frac{V\mu}{Ib} = 10,5MPa < \tau_{adm}$
2) $\frac{M}{W} + \frac{N}{A} = 90,4MPa < \sigma_{adm}$
3) $\frac{M}{W} + \frac{N}{A} = 111,5MPa < \sigma_{adm}$

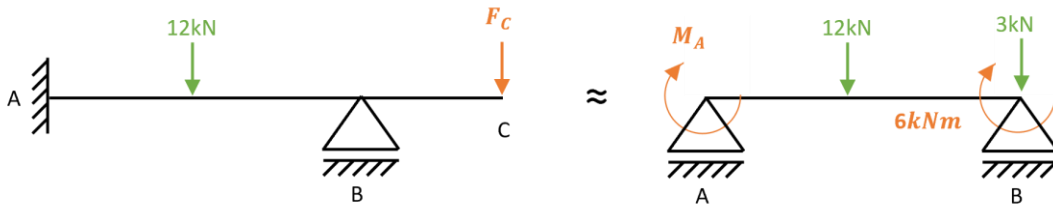
Dimensiono con **PNI 220**.

Ejercicio 2

Parte A



$$F_C = F_D = 3kN$$

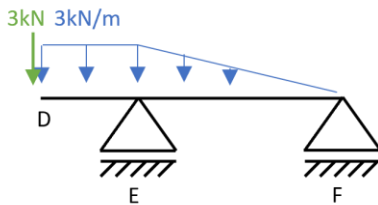


$$\theta_A = \frac{M_A \cdot 4m}{3EI} - \frac{6kNm \cdot 4m}{6EI} + \frac{12kN \cdot (4m)^2}{16EI} = 0$$

$$\Rightarrow M_A = \frac{6kNm}{2} - \frac{3 \cdot 12kN \cdot 4m}{16} = -6kNm$$

$$\Sigma M_A = 0 \Rightarrow M_A + V_B \cdot 4m = 3kN \cdot 6m + 12kN \cdot 2m \Rightarrow V_B = 9kN$$

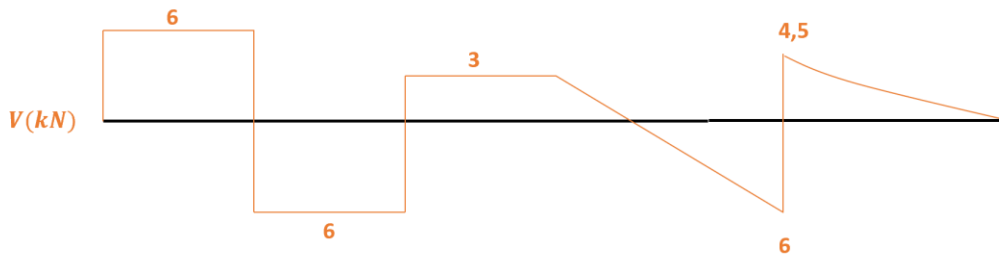
$$\Sigma F_V = 0 \Rightarrow V_A = 12kN + 3kN - V_B = 6kN$$

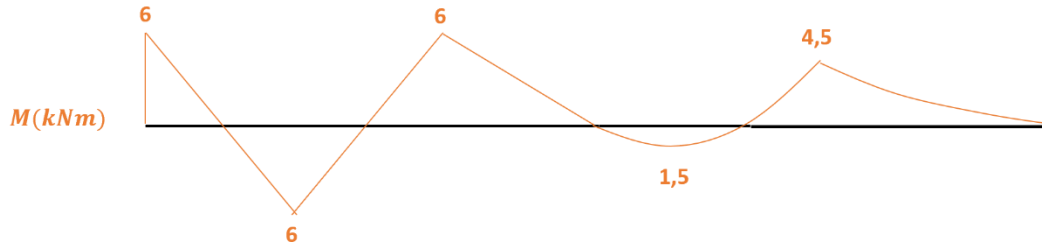


$$\Sigma M_F = 0 \Rightarrow V_E \cdot 3m = 3kN \cdot 4m + \frac{3kN}{m} \cdot 1m \cdot 3,5m + \frac{3kN}{m} \cdot \frac{3m}{2} \cdot 2m \Rightarrow V_E = 10,5kN$$

$$\Sigma F_V = 0 \Rightarrow V_F = \frac{3kN}{m} \cdot 1m + \frac{3kN}{m} \cdot \frac{3m}{2} + 3kN - V_E = 0kN$$

Parte B





Parte C

$$n = \frac{E_{madera}}{E_{acero}} = \frac{10GPa}{210GPa} = \frac{1}{21}$$

$$y_G = \frac{15cm \cdot 1cm \cdot 20,5cm + 1cm \cdot 20cm \cdot 10cm}{35cm^2} = 14,5cm$$

$$I_h = \frac{15cm \cdot (1cm)^3}{12} + \frac{1cm \cdot (20cm)^3}{12} + 15cm \cdot 1cm \cdot (6cm)^2 + 20cm \cdot 1cm \cdot (4,5cm)^2 = 1613cm^4$$

$$y_{sup} = 21cm - y_G = 6,5cm \quad y_G = y_{inf}$$

$$W_{sup} = \frac{I_h}{y_{sup}} = 248cm^3 \quad W_{inf} = \frac{I_h}{y_{inf}} = 111cm^3$$

$$\sigma_{max,acero} = \frac{M_{max}}{W_{sup}} = \frac{6kNm}{248cm^3} = 24MPa < 140MPa$$

$$\sigma_{C,max,madera} = \sigma_{T,max,madera} = \frac{M_{max}}{W_{inf}} \cdot n = \frac{6kNm}{111cm^3} \cdot \frac{1}{21} = 2,57MPa < 3MPa$$

Parte D

$$\mu_G = 15cm \cdot 1cm \cdot (20,5cm - 14,5cm) = 90cm^3$$

$$\tau_b = \frac{V_{max} \mu_G}{I_h} = 33,48kN/m$$

$$\tau_{adm} \geq \frac{F_{conector}}{A_{conector}} = \frac{\tau_b s}{2A_{conector}} = \frac{\tau_b s}{2 \left(\frac{\pi \phi^2}{4} \right)} \Rightarrow \phi \geq \sqrt{\frac{2\tau_b s}{\pi \tau_{adm}}} = 7,8mm$$

$$\Rightarrow \phi = 8mm$$