

Examen de Electrónica 2
20/02/2006



50709867

Resolver cada problema en hojas separadas.

Duración de la prueba: 3 horas 30 minutos.

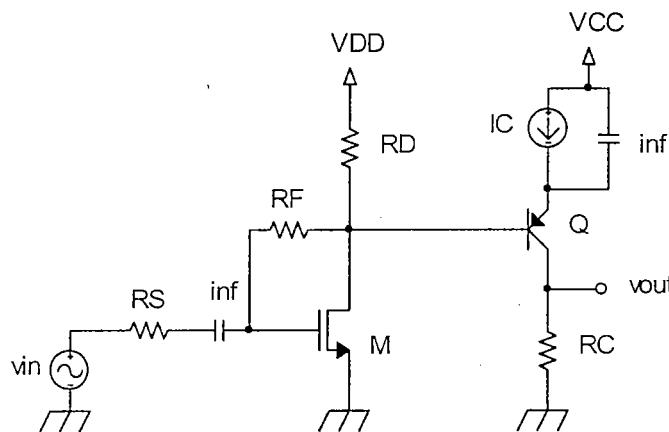
La prueba es sin material.

Los puntajes de los problemas se indican sobre un total de 100 puntos.

**Problema 1 (37 ptos):**

En el amplificador de la Figura determinar:

- Ganancia a frecuencias medias
- Frecuencia de corte superior

**Datos:**

$$VCC = VDD = 3V \quad IC = 0.1mA$$

$$RC = 6.8k \quad RD = 6.8k \quad RF = 10M \quad RS = 1k$$

$$M: VT = 1V \quad \delta = 0 \quad \mu Cox(W/L) = 10 \text{ mA/V}^2 \quad C_{gs} = C_{gd} = 1pF$$

$$Q: V_{EB} = 0.7V \quad \beta = 200 \quad C_{\mu} = 0.8pF \quad C_{je} = 5pF \quad f_T @ 10mA = 6GHz$$

Problema 2 (37 ptos):

Dado el amplificador de la figura 1:

- ¿qué condición debe darse en el circuito para que los diodos D1 y D2 conduzcan? ¿Cuál es, entonces, la función de estos diodos?
- dar las corrientes de polarización de los transistores Q8, Q9, Q12, Q13, Q16, Q17;
- calcular la ganancia a bajas frecuencias;
- determinar el f_T

Datos:

$$V_{DD} = V_{EE} = 18V$$

$$V_{BE} = |V_{EB}| = V_\gamma = 0.7V$$

$$V_{CEsat} = 0.2V$$

Tensión de Early = ∞ , excepto en el transistor Q13 donde $V_A = 30V$

$\beta = 100$ excepto en Q14 y Q20 donde $\beta = 50$.

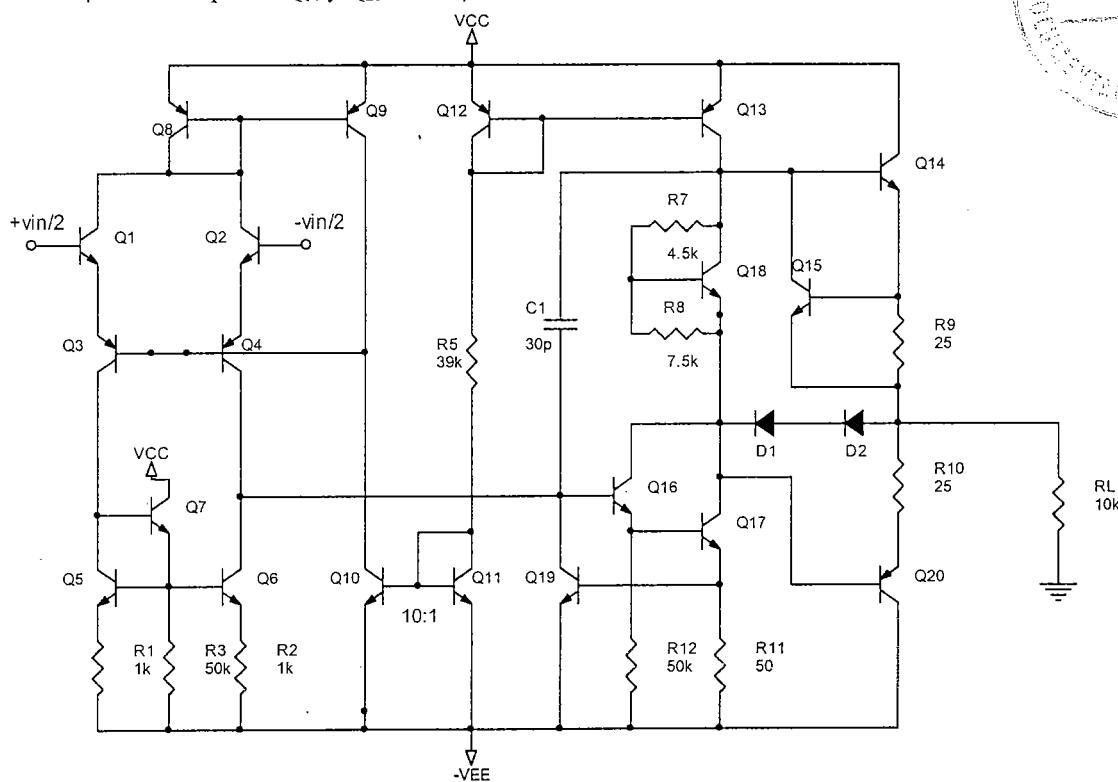


Fig.1

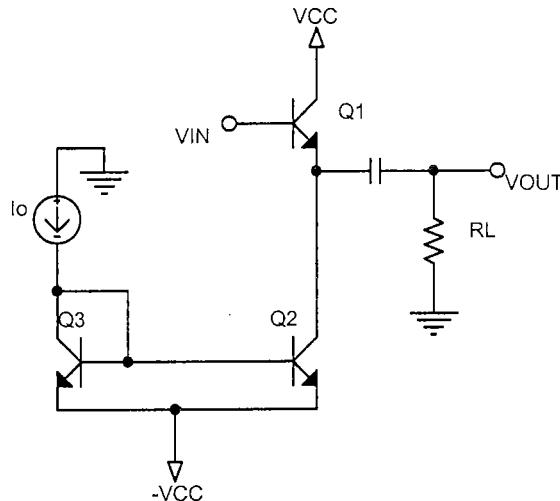
Pregunta (26 ptos):

- Para la etapa de potencia de la figura, determinar la máxima eficiencia que sería posible alcanzar para una señal de entrada sinusoidal, indicando bajo qué condiciones se alcanzaría esta eficiencia máxima.
- En el caso particular en que $V_{CC} = 5V$, $I_o = 1A$, $RL = 4\Omega$, $V_{opico} = 2V$, V_{BE} para todos los transistores es $0.8V$ y el nivel de continua en V_{IN} es $0.8V$, determinar, la potencia entregada a la carga, el rendimiento y la potencia disipada por cada uno de los transistores Q1, Q2 y Q3.
- Se implementa el circuito con transistores TIP 41, de los que se adjuntan datos y se considerará que la tensión base-emisor es de $0.8V$. Se desea que el circuito opere con una temperatura ambiente máxima de $45^\circ C$ y se está en las condiciones de la parte b).
 - Indicar para cada transistor si se requiere utilizar un disipador, explicando claramente porqué si o porqué no y que datos de la hoja de datos utiliza para deducir esto.
 - Para los transistores que se requiera utilizar un disipador, se desea utilizar el mismo para todos. Determinar que condición debe cumplir su resistencia térmica disipador –

3142

ambiente si se monta de modo que la resistencia térmica disipador – carcaza del dispositivo (“case”) es $0.5^{\circ}\text{C}/\text{W}$.

NOTA: Se despreciará en todo el problema la potencia disipada debido a las corrientes de base de los transistores.



Complementary Silicon Plastic Power Transistors

... designed for use in general purpose amplifier and switching applications.

- Collector-Emitter Saturation Voltage —
 $V_{CE(sat)} = 1.5 \text{ Vdc} (\text{Max}) @ I_C = 6.0 \text{ Adc}$
- Collector-Emitter Sustaining Voltage —
 $V_{CEO(sus)} = 80 \text{ Vdc} (\text{Min}) — \text{TIP41A, TIP42A}$
 $= 80 \text{ Vdc} (\text{Min}) — \text{TIP41B, TIP42B}$
 $= 100 \text{ Vdc} (\text{Min}) — \text{TIP41C, TIP42C}$
- High Current Gain — Bandwidth Product
 $f_T = 3.0 \text{ MHz} (\text{Min}) @ I_C = 500 \text{ mAdc}$
- Compact TO-220 AB Package.

*MAXIMUM RATINGS

Rating	Symbol	TIP41A TIP42A	TIP41B TIP42B	TIP41C TIP42C	Unit
Collector-Emitter Voltage	V_{CEO}	60	60	100	Vdc
Collector-Base Voltage	V_{CB}	60	60	100	Vdc
Emitter-Base Voltage	V_{EB}		5.0		Vdc
Collector Current — Continuous Peak	I_C		5	10	Adc
Base Current	I_B		2.0		Adc
Total Power Dissipation $@ T_C = 25^{\circ}\text{C}$ Derates above 25°C	P_D		65	0.52	Watts $\text{W}/^{\circ}\text{C}$
Total Power Dissipation $@ T_A = 25^{\circ}\text{C}$ Derates above 25°C	P_D		2.0	0.016	Watts $\text{W}/^{\circ}\text{C}$
Undamped Inductive Load Energy (1)	E		62.5		mJ
Operating and Storage Junction Temperature Range	$T_J, T_{Storage}$	$-65 \text{ to } +150$			$^{\circ}\text{C}$

THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Ambient	R_{JA}	62.5	$^{\circ}\text{C}/\text{W}$
Thermal Resistance, Junction to Case	R_{JC}	1.52	$^{\circ}\text{C}/\text{W}$

(1) $I_C = 2.5 \text{ A}, L = 20 \text{ mH}, \text{P.R.F.} = 10 \text{ Hz}, V_{CC} = 10 \text{ V}, R_{BE} = 100 \Omega$

NPN
TIP41A
TIP41B*
TIP41C*
PNP
TIP42A
TIP42B*
TIP42C*

*Motorola Preferred Device

6 AMPERE
POWER TRANSISTORS
COMPLEMENTARY
SILICON
60-80-100 VOLTS
65 WATTS



CASE 221A-06
TO-220AB

Examen Electrónica 2

2012 / 06

Problema 1

a) Ganancia a frecuencias medianas

DC:

$$\bullet I_{CQ} = I_C = 0.1 \text{ mA} \rightarrow \left\{ \begin{array}{l} g_{mQ} = \frac{I_C}{V_T} = 3.8 \text{ mS} \\ r_\pi = 52 \text{ k} \end{array} \right.$$

$$\bullet I_{DQ} = I_D = 0.5 \text{ mA} \quad (V_Q - V_T)^2 \quad (1) \quad V_S = 0, \quad K = \mu C_{ox} \frac{w}{L}$$

$$I_D = \frac{V_{DD} - V_Q}{R_D} \rightarrow V_Q = V_{DD} - I_D R_D \quad (2)$$

$$\text{De (1) y (2): } 0.5K \cdot R_D^2 I_D^2 - (1 + K(V_{DD} - V_T) \cdot R_D) \cdot I_D + 0.5K \cdot (V_{DD} - V_T)^2 =$$

$$\text{Hay 2 soluciones: } I_{D1} = 0.33 \text{ mA}$$

$$I_{D2} = 0.26 \text{ mA}$$

$V_Q = V_S$ porque por RF no circula corriente en dc \rightarrow necesariamente el transistor debe estar en saturación $\rightarrow V_{Q2} > V_T$

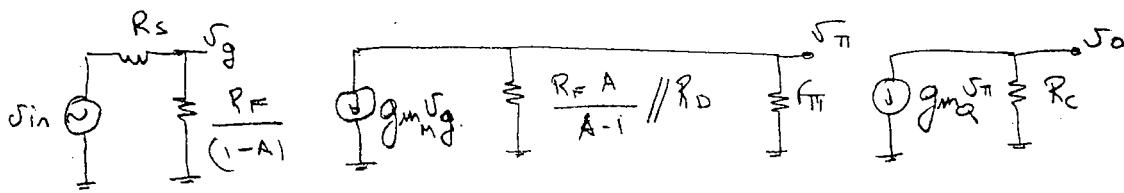
$$\text{Para } I_{D1} \rightarrow V_{Q1} = V_{DD} - I_{D1} R_D = 0.25 \text{ V} < V_T \quad \times$$

$$\rightarrow I_{D2} \rightarrow V_{Q2} = 1.2 \text{ V} > V_T \quad \checkmark \quad \leftarrow I_D = 0.26 \text{ mA}$$

R. Fornell

5.1.3

A) Frecuencias medias:



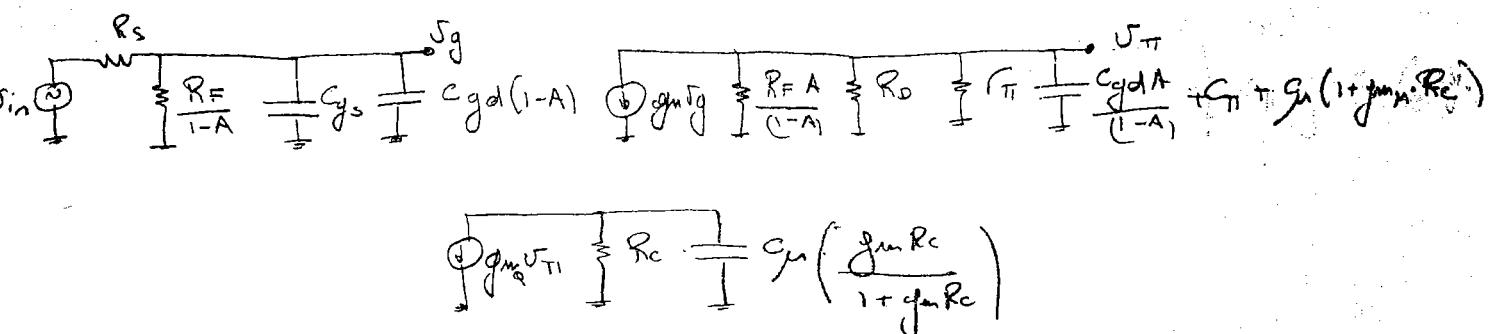
$$A = \frac{V_\pi}{V_g}$$

$$V_\pi \approx g_{mN} r_\pi // R_F // R_D \approx g_{mN} r_\pi // R_D \Rightarrow A = -13.$$

Siendo
 $A \gg 1$

$$A_{\text{Tot}} = \frac{V_o}{V_g} = A \cdot \underbrace{\left(-g_{mQ} R_c \right)}_{V_\pi / V_g = 26} = \underline{33.8 \text{ V/V}}$$

b) Frecuencia de corte superior: Aplico Miller a C_{gd} y C_{T1}



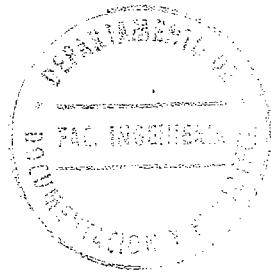
$$f_1 = \frac{1}{2\pi \cdot R_s \cdot \left(C_{gs} + C_{gd} \cdot \frac{1}{1-A} \right)} = 10,6 \text{ MHz}$$

$$f_2 = \frac{1}{2\pi \cdot R_D // r_\pi \cdot \left(C_{gd} + C_{T1} + C_m \cdot \left(1 + g_{mN} R_c \right) \right)} = \boxed{0.95 \text{ MHz} = f_{-3dB}}$$

$$f_3 = \frac{1}{2\pi R_c C_m} = 29 \text{ MHz}$$



Záluží de C_{π} :



$$f_{\pi} @ 10mA = \frac{g_{me@10mA}}{2\pi(C_{\pi} + C_{\mu})}$$

$$g_{me@10mA} = 0,38 S.$$

$$2\pi(C_{\pi} + C_{\mu}) = \frac{g_{me@10mA}}{f_{re,0mA}} = 64 \times 10^{-12} \rightarrow C_{\pi} @ 10mA = \frac{64 \times 10^{-2}}{2\pi} - C_{\mu} = 1,9 \times 10^{-12}$$

$$C_{\pi} @ 10mA = C_{je} + \alpha \frac{I_c}{10mA} \Rightarrow \alpha = 0,44 \times 10^{-9} \rightarrow C_{\pi} @ 10mA = C_{je} + \alpha \cdot 1mA = 5,44 pF$$

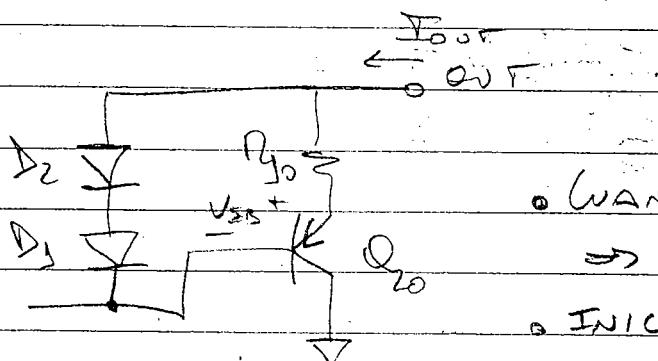
R. Barelli

EXAMEN ELECTRÓNICA 2

20/02/2006

(2)

(a)



- Cuando I_{out} entra
- $\Rightarrow Q_{20}$ está ON
- INICIALMENTE D_1 , D_2 están OFF

$$\rightarrow 2V_x = R_{10} I_{E20} + V_{BE20} \quad D_1, D_2 \text{ están } \Delta \text{ ON}$$

$$\Rightarrow I_{E20} = \frac{V_x}{R_{10}} = 28 \text{ mA} \quad | \quad \text{condición}$$

Tienen la función de proteger el amplificador contra sobrecorrientes o saturación.

Mientras D_1 , D_2 estén OFF $I_{out} = I_{E20}$

Entonces $I_{E20} = V_x / R_{10} = 28 \text{ mA}$, entonces a circular el exceso de I_{out} por los diodos hacia Q_{10} y Q_{17} , hasta que la tensión a través de R_{10} es igual a V_{BE} . Ahí

Q_{10} se enciende y comienza a circular por la base de $Q_{10} \Rightarrow V_{B10} \downarrow \Rightarrow V_{C10} = V_{C17} \uparrow$

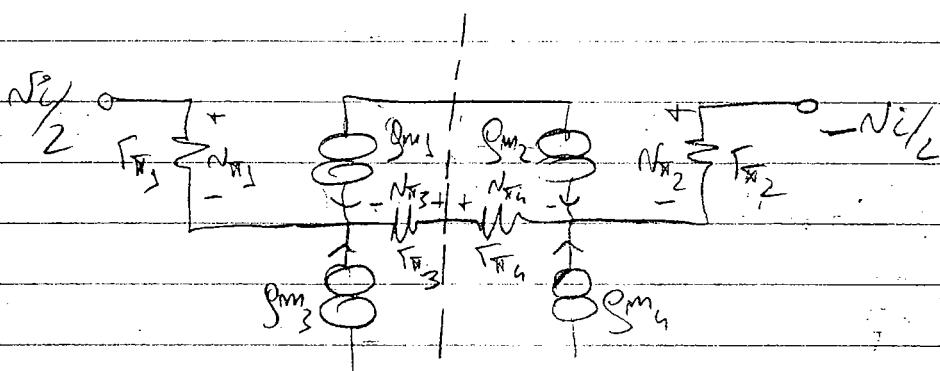
$$\Rightarrow V_{B10} \uparrow \Rightarrow V_{out} \uparrow \Rightarrow I_{out} \downarrow$$

$$(b) I_{C12} = I_{C13} = b I_{C10} ; \quad I_{C10} = I_{C9} = I_{C8}$$

$$I_{C12} = \frac{V_{CC} + V_{BE} - 2V_{BE}}{R_S} = 0,89 \text{ mA} \quad |$$

$$\Rightarrow I_{C10} = 89 \mu \text{A} \quad |$$

(c) Etapa de enfoque:



es decir $f_{T1} \approx (f_{T1} = f_{T2} = f_{T3} = f_{T4})$ y con enfoque

$$\text{diferencial} \Rightarrow N_{T1} - N_{T3} = N_{\text{c}}/2$$

$$\Delta \text{tensos } R_{T1} = R_{T3} \quad \text{y } C_{m1} = C_{m3}$$

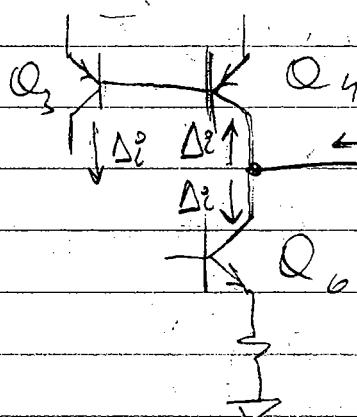
$$\Rightarrow N_{T3} = -R_{T3}(C_{m3}N_{T1} + C_{m1}N_{T3})$$

$$\Rightarrow \underbrace{(1 + C_{m3}R_{T3})}_{B+} N_{T3} = -\underbrace{C_{m3}R_{T3}N_{T1}}_B$$

$$\Rightarrow N_{T3} = -N_{T1} \Rightarrow N_{T3} - N_{T1} = -2N_{T3} = N_{\text{c}}/2$$

$$\Rightarrow i_{C3} = C_{m3}N_{T3} = -C_{m3}N_{\text{c}}/2$$

$Q_5, Q_6 \rightarrow Q_7$ son un eje



$$\Delta_i = C_{m3}N_{\text{c}}/2$$

$$\Rightarrow i_{Q5} = C_{m3}N_{\text{c}}/2 \Rightarrow C_{m3} = C_{m1} = C_{m2}$$

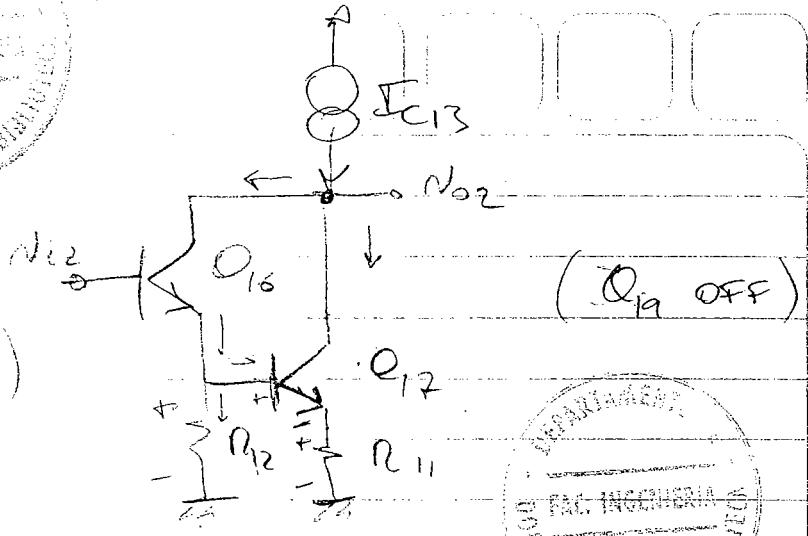
$$R_Q = \infty \Rightarrow i_{Q5} = \infty$$

$$\Rightarrow G_{M3} = \frac{1}{2} \left(\frac{i_{C3}}{2V_T} \right) \Rightarrow G_{M3} = 9.86 \text{ mA/V}$$

2^{do} etapa

$$R_{C2} = r_{E16} + \beta(R_{B17} // R_{12})$$

$$R_{B17} = r_{E12} + \beta R_{11}$$



$$I_{E16} + I_{C17} = I_{C13} \quad (\text{diferencia } I_{B12})$$

$$I_{C16} - \frac{I_{C17}}{\beta} \times R_{12} = V_{BE17} + I_{C17} R_{11} \quad (\text{No topeo de } I_{B12})$$

$$I_{C13} R_{12} = V_{BE17} + I_{C17} \left(R_{11} + R_{12} \frac{\beta+1}{\beta} \right)$$

$$\Rightarrow I_{C17} = I_{C13} \frac{R_{12}}{R_{11} + R_{12} \frac{\beta+1}{\beta}} - \frac{V_{BE}}{R_{11} + \frac{\beta+1}{\beta} R_{12}}$$

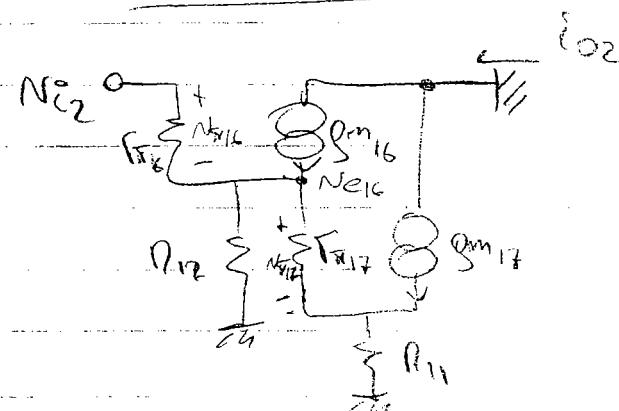
$$\Rightarrow I_{C17} = 0,866 \text{ mA}$$

$$\Rightarrow I_{C16} = 24 \mu A \quad \checkmark \quad I_{B17} = 8,66 \mu A \quad \checkmark$$

$$r_{E16} = 158 \text{ m}\Omega$$

$$r_{E17} = 3 \text{ m}\Omega \Rightarrow R_{B17} = 8 \text{ m}\Omega$$

$$\Rightarrow R_{C2} = 798 \text{ m}\Omega$$



$$I_{C2} = g_m I_{E16} N_{E16} + g_m I_{E17} N_{E17}$$

$$N_{E16} = \frac{r_{E16}}{r_{E16} + \beta(R_{B17} // R_{12})} N_{C2}$$

$$N_{E17} = \frac{r_{E17}}{r_{E17} + \beta R_{11}} \frac{(N_{C2} - N_{E16})}{r_{E16}}$$

$$N_{T12} = \frac{f_{T17}}{f_{T16} + \beta R_{11}} \times \frac{\beta (R_{VB17} // R_{12})}{f_{T16} + \beta (R_{VB12} // R_{12})} N_{i2}$$

$$\Rightarrow \text{Corr}_2 = \left[\frac{\beta}{f_{T16} + \beta (R_{VB12} // R_{12})} + \frac{\beta^2 (R_{VB17} // R_{12})}{(f_{T17} + \beta R_{11})(f_{T16} + \beta (R_{VB12} // R_{12}))} \right] N_{i2}$$

$$\text{Corr}_2 = \frac{\beta N_{i2}}{f_{T16} + \beta (R_{VB12} // R_{12})} \left\{ 1 + \frac{\beta (R_{VB17} // R_{12})}{f_{T17} + \beta R_{11}} \right\} \\ R_{E2}$$

$$\Rightarrow \text{Corr} = \frac{\beta}{N_{i2}} \left[1 + \frac{\beta R_{12}}{R_{VB12} + R_{12}} \right] N_{i2}$$

$$\frac{\text{Corr}}{N_{i2}} = Gm_2 = 10,9 \text{ mA/V}$$

$$R_{o2} = f_{T13} = 33,7 \text{ k}\Omega \quad (\text{despre os } R_V) \\ (\text{mult. de } V_{BE})$$

3º etapa (sup. R_{22} on; on R_{14} e identico)

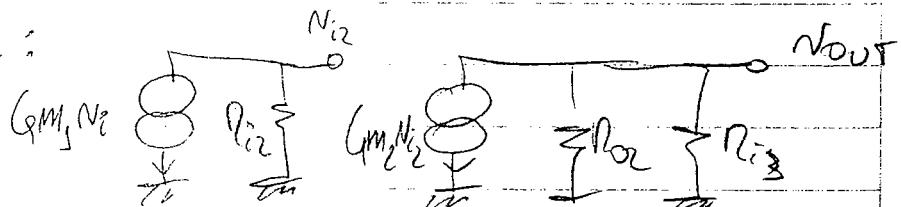
$$R_{i3} = \beta_{22}(R_{33} + R_L) \approx \beta_{22} R_L = 500 \text{ k}\Omega$$

$A_3 \approx 1$ sempre q' $Gm_3 R_L \gg 1$ (segundo)

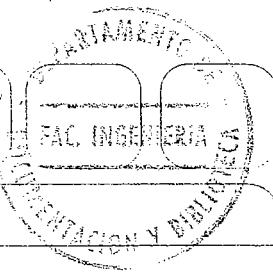
(obs condicão se cplle $\Leftrightarrow T_{C22} \geq \frac{10V}{R_L} = 2,16 \mu\text{A}$)

\Rightarrow Esquema Pôlo:

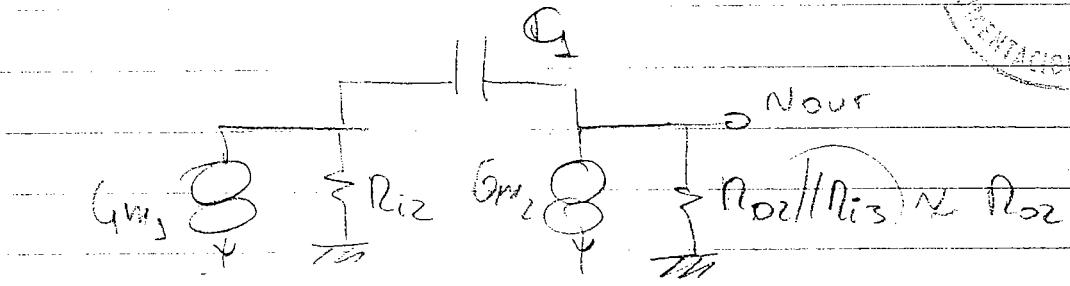
(R_{13} Freq.)



$$\Rightarrow A_0 = Gm_1 R_{i2} Gm_2 (R_{12} // R_{i3}) = 1250 \text{ mA/V}$$



(1)



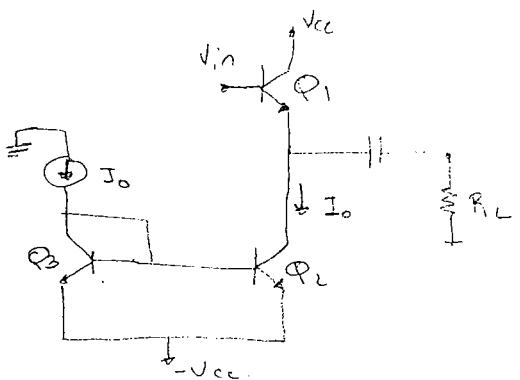
$$\omega_T = \Delta_0 \omega_{3dB}$$

$$(x' \pi \eta_1 \eta_2) \omega_{3dB} = \frac{1}{R_{1z} C_1 Gm_2 R_{2z}} \quad (Gm_2 R_{2z} \gg 1)$$

$$\Rightarrow \omega_T = \frac{Gm_1 R_{1z} Gm_2 R_{2z}}{R_{1z} C_1 Gm_2 R_{2z}} = \frac{Gm_1}{C_1}$$

$$\Rightarrow f_T = 4,54 \text{ MHz}$$

Pregunta



$$\eta = \frac{P_L}{P_S}$$

$$P_L = \frac{\hat{V}_o^2}{2R_L}$$

$$P_{S+} = V_{cc} \cdot I_o$$

$$P_{S-} = 2V_{cc}I_o$$

$$\eta = \frac{\hat{V}_o^2}{6 \cdot V_{cc} I_o R_L} = \frac{1}{6} \cdot \frac{\hat{V}_o}{V_{cc}} \cdot \frac{\hat{V}_o}{R_L I_o}$$

La eficiencia máxima se alcanza cuando $\hat{V}_o = V_{cc}$ y $R_L = \frac{V_{cc}}{I_o} = \hat{V}_o$

En este caso $\eta = 1/6$

b)

$$V_{cc} = 5V$$

$$I_o = 1A$$

$$R_L = 5\Omega$$

$$\hat{V}_o = 2V$$

$$V_{BE} = 0.8$$

$$P_L = \frac{\hat{V}_o^2}{2R_L} = 0.5W$$

$$\eta = \frac{1}{6} \cdot \frac{1}{6} \cdot \frac{2}{5} = 0.033 \rightarrow 3.3\%$$

$$P_D = P_{S+} + P_{S-} - P_L = 3 \cdot V_{cc} \cdot I_o - P_L = 14.5W$$

$$P_{DQ_3} = V_{BE} \cdot I_o = 0.8W$$

$$P_{DQ_2} = V_{cc} \cdot I_o = 5W$$

$$P_D^{\text{comap}_1} = P_{S+} + P_{S-} - P_L = 9.5W$$

$$P_D^{\text{comap}_2} = P_{Q_1} + P_{Q_2}$$

$$\frac{P_{DQ_1}}{P_D^{\text{comap}_1}} = 4.5W$$

c)

$$T_{amb} = 45^\circ C$$



a) $T_{amb} + R_{oja} \cdot P_D = T_j$

$$Q_3: 45^\circ C + 62,5 \text{ } ^\circ C/W \cdot 8W = 95^\circ C < T_j^{max} = 150^\circ C$$

\hookrightarrow No es necesario

$$Q_1, Q_2: 45^\circ C + 62,5 \text{ } ^\circ C/W \cdot 5W = 358^\circ C > T_j^{max}$$

\hookrightarrow Es necesario.

De la hoja de datos se utilizan los sig. datos: R_{oja} , T_j .

b)

$$T_{amb} + (R_{oja} + R_{ocv} + R_{oda}) \cdot P_D < T_j^{max} - \text{Tomo el transistor p1}$$

esta más diñitado: Φ_2

$$R_{oda} < \frac{(T_j^{max} - T_{amb})}{P_D} - R_{oja} - R_{ocv} = \underline{\underline{18.6 \text{ } ^\circ C/W}}$$

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