

1er Parcial 2019 - SOLUCION

Parte (a)

	P(kW)	Q(kVar)	cos φ	S(kVA)
TF1	200,0	118,7	0,86	232,6
TIL1	90	26,3	0,96	93,8
TF2	120	30,1	0,97	123,7
TF3	200,0	118,7	0,86	232,6
TIL2	90	26,3	0,96	93,8
	700,0	319,9	Sdem	769,6

Id\_motores(A)

178,6

Parte (b)

Sdem=	769,6	kVA	
x1,1	846,6	kVA	, por lo tanto, Smin= 846,6

Se debe seleccionar trafo de 1000kVA y ucc=6%

Parte (c)

	P(kW)	Q(kVar)	cos φ	S(kVA)	In(A)
MOTOR	30	7,5	0,97	30,9	44,64 (=Id_motor)

$$\Rightarrow \Delta U \approx \sqrt{3}(RI \cos \varphi + XI \sin \varphi)$$

L=	40	m
Id=	44,64	A
R=	0,05625	Ω
X=	0,004	Ω
cos φ	0,97	
sen φ	0,24	
ΔU2	4,29	V

GPO MOTORES	PL(kW)	QL(kVar)
	127,5	32,0

SL(kVA)	IL(A)
131,4	189,72

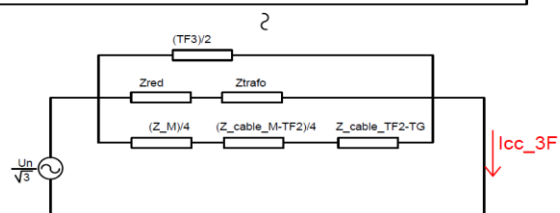
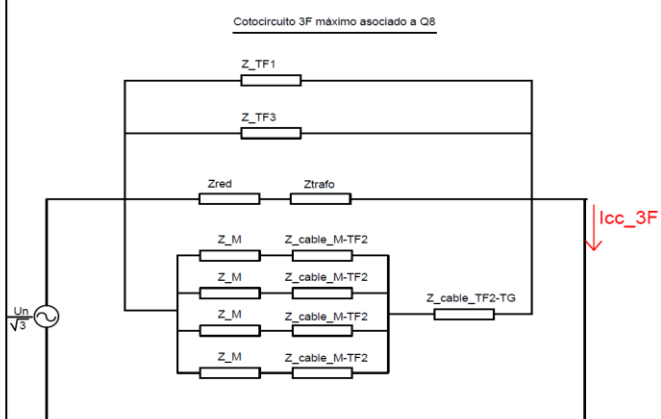
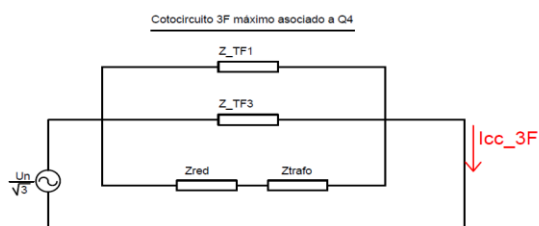
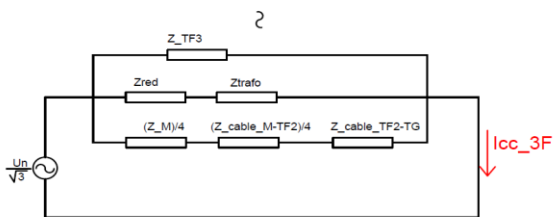
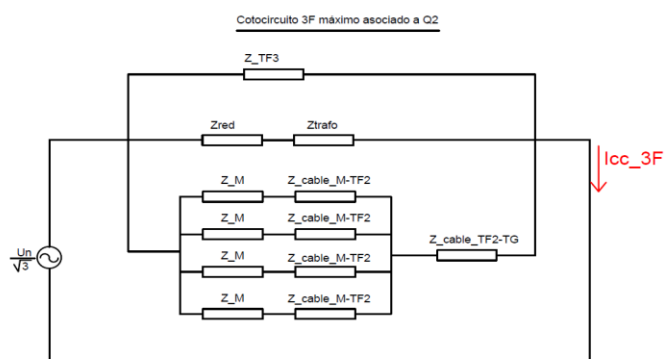
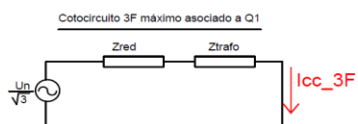
fa=	0,75
ft=	1,08
(fa x ft)	0,81

S(mm2)	Itabla(A)	Iz(A)
70	185	149,9
95	224	181,4
120	260	210,6
150	299	242,2
185	341	276,2

L=	80	m
Id=	178,56	A
R=	0,015	Ω
X=	0,008	Ω
cos φ	0,97	
sen φ	0,24	
ΔU1	5,10	V

Δ-ACUM=	ΔU1+ΔU2 =	9,40	V
	Δ-ACUM/Unx100 =	2,3%	< 5%(FM)

Parte (d)



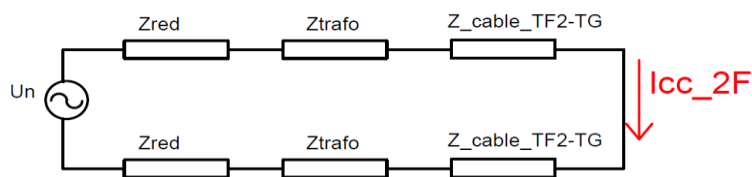
Un_BT	400	V	
RED	Un_MT	31,5	kV
	Icc	16	kA
	Sc	873,0	MVA
	Zred=	0,183285799742738i	mΩ
TRAFO	Sn	1000	kVA
	ucc=	6%	
	Ztrafo=	9,6i	mΩ
MOTOR	Sn	30,9	kVA
	xm	20%	
	Zm=	1034,66666666667i	mΩ
	Zm/4=	258,666666666667i	mΩ
Cable TG-TF2	Rc=	15	mΩ
	Xc=	8	mΩ
	Zc_TG-TF2=	15+8i	mΩ
Cable TF2-Motor	Rc=	56,25	mΩ
	Xc=	4	mΩ
	Zc_TF2-Motor=	56,25+4i	mΩ
	Zc_TF2-Motor/4=	14,0625+i	mΩ
Tablero TF3=TF1	S=	232,6	kVA
	xm	20%	
	Z_TF3=	137,6i	mΩ
	Z_TF3/2=	68,8i	mΩ

(Zred+Ztrafo)	9,78328579974274i	mΩ				
Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2 =	29,0625+267,666666666667i	mΩ				
icc_3F_max_Q1=	23,61	kA	, por lo tanto,	PdC_Q1>	23,61	kA
Zequiv	9,8	mΩ				
(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2)/(Zred+Ztrafo)					0,0357432383562878+9,4420570760284i	
(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2) x (Zred+Ztrafo)					-2618,65949906448+284,326743555023i	
(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2) + (Zred+Ztrafo)					29,0625+277,44995246641i	
(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2)/(Zred+Ztrafo)//ZTF3					0,0313002351231508+8,83575895406244i	
[(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2)/(Zred+Ztrafo)] x ZTF3					-1299,227053666151+4,9182695978252i	
[(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2)/(Zred+Ztrafo)] + ZTF3					0,0357432383562878+147,042057076028i	
icc_3F_max_Q2=	26,14	kA	, por lo tanto,	PdC_Q2>	26,14	kA
Zequiv	8,8	mΩ				
(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2)/(Zred+Ztrafo)//(ZTF3/2)					0,0276369531936507+8,30262570977299i	
[(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2)/(Zred+Ztrafo)] x (ZTF3/2)					-649,613526830754+2,4591347989126i	
[(Zm/4 + Zc_TF2-Motor/4 + Zc_TG-TF2)/(Zred+Ztrafo)] + (ZTF3/2)					0,0357432383562878+78,2420570760284i	
icc_3F_max_Q8=	27,82	kA	, por lo tanto,	PdC_Q8>	27,82	kA
Zequiv	8,3	mΩ				
(TF3/2)/(Zred+Ztrafo)	8,56530820991078i					
(TF3/2) x (Zred+Ztrafo)	-673,090063022301					
(TF3/2) + (Zred+Ztrafo)	78,5832857997427i					
icc_3F_max_Q4=	26,96	kA	, por lo tanto,	PdC_Q4>	26,96	kA
Zequiv	8,6	mΩ				

Parte (e)

- 1)  $I_L < I_r_{Q4} < I_z$  -----> **189,7 A < I\_r\_{Q4} < 210,6 A**
- 2)  $PdC_{Q4} > I_{cc\_m\acute{a}x}$  -----> **PdC\_Q4 > 26,96kA**
- 3)  $I_m_{Q4} < I_{cc\_m\acute{i}n}$  -----> **I\_m\_Q4 < 8,6kA**

Cotocircuito 2F m\acute{i}nimo asociado a Q4



(Zred+Ztrafo+Z_cable_TF2-TG)	15+17,7832857997427i	mΩ
Zred+Ztrafo+Z_cable_TF2-TG	23,26	mΩ
icc_2F_m\acute{i}n=	8,60	kA