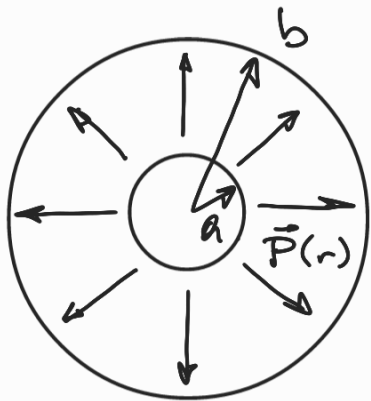


1

$$\vec{P}(r) = \frac{k}{r} \hat{e}_r \quad a \leq r \leq b$$



a) coords. esféricas;  $\vec{P} = P(r) \hat{e}_r$

$$\rho_p = -\nabla \cdot \vec{P} = -\frac{1}{r^2} \frac{d(r^2 P(r))}{dr} = -\frac{1}{r^2} \frac{d}{dr} \left( r^2 \frac{k}{r} \right) = -\frac{k}{r^2}$$

$\rho_p(r)$  para  $a < r < b$

$$\sigma_p|_a = P \cdot \hat{n} \Big|_{r=a} = -\frac{k}{a} \quad \sigma_p|_b = P \cdot \hat{n} \Big|_{r=b} = \frac{k}{b}$$

$$Q_p = \int_V \rho_p dV + \int_{S_a} \sigma_p|_a dS + \int_{S_b} \sigma_p|_b dS = -4\pi k(b-a) - 4\pi k a + 4\pi k b = 0$$

$\int_a^b -k \frac{4\pi r^2}{r^2} dr = -4\pi k(b-a)$      $-\frac{k}{a} 4\pi a^2$      $\frac{k}{b} 4\pi b^2$

b)  $\vec{D} = 0, \forall r$  no hay cargas libres ( $\nabla \cdot \vec{D} = \rho_L = 0$ )

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}$$

con  $\begin{cases} P = 0 & ; r < a \text{ y } r > b \\ P = \frac{k}{r} \hat{e}_r & ; a \leq r \leq b \end{cases}$

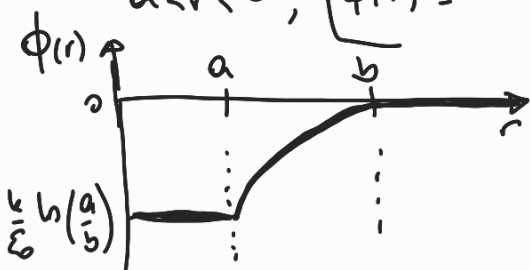
$$\vec{E} = E(r) \hat{e}_r$$

$$\Rightarrow \vec{E} = \begin{cases} 0 & r < a \\ -\frac{P(r)}{\epsilon_0} = -\frac{k}{\epsilon_0 r} \hat{e}_r & a \leq r \leq b \\ 0 & r > b \end{cases}$$

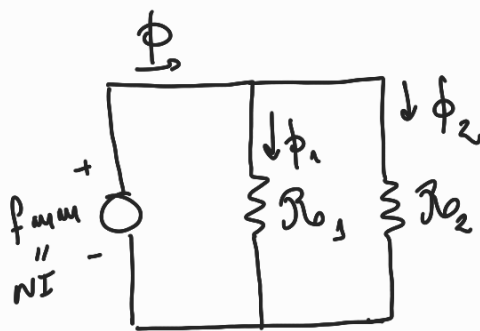
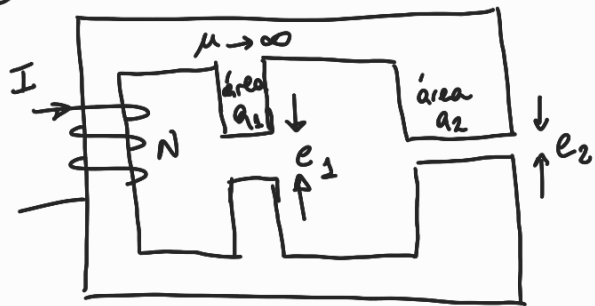
Para  $r < a$ ;  $\phi(r) = -\int_{\infty}^r E dr = -\int_{\infty}^b E dr - \int_b^a -\frac{k}{\epsilon_0 r} dr - \int_a^r 0 dr = \frac{k}{\epsilon_0} \ln\left(\frac{a}{b}\right)$

$r > b$ ;  $\phi(r) = -\int_{\infty}^r E dr = 0$

$a < r < b$ ;  $\phi(r) = -\int_{\infty}^r E dr = -\int_{\infty}^b E dr - \int_b^r -\frac{k}{\epsilon_0 r} dr = \frac{k}{\epsilon_0} \ln\left(\frac{r}{b}\right)$



2



En los tramos donde la permeabilidad es infinita ( $\mu \rightarrow \infty$ ), la reluctancia tiende a cero ya que es proporcional al inverso de  $\mu$ .

Entonces, en la rama izquierda, donde está el enrollado, la reluctancia es nula ( $R_{01} = 0$ ), mientras que en las ramas central y derecha sólo aportan a las reluctancias las regiones con entrehierros.

rama central  $R_{01} = \frac{e_1}{\mu_0 a_1}$  y rama derecha  $R_{02} = \frac{e_2}{\mu_0 a_2}$

Ampere  $\rightarrow NI = \phi R_{01} + \phi_1 R_{01}$  (recorro rama izquierda y central)  
 $NI = \phi R_{01} + \phi_2 R_{02}$  ( " " " " derecha)  
 $\phi = \phi_1 + \phi_2$   
 $\phi_1 = \frac{NI}{R_{01}}$   
 $\phi_2 = \frac{NI}{R_{02}}$

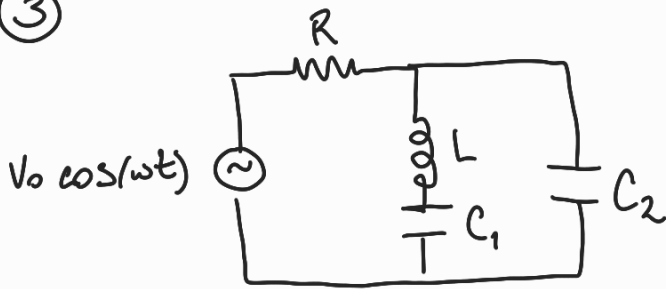
$$\phi = \phi_1 + \phi_2 = NI \left( \frac{1}{R_{01}} + \frac{1}{R_{02}} \right) = NI \left( \frac{R_{01} + R_{02}}{R_{01} R_{02}} \right)$$

$$L = N \frac{d\phi}{dI} = N^2 \left( \frac{R_{01} + R_{02}}{R_{01} R_{02}} \right) = N^2 \left( \frac{\frac{e_1}{\mu_0 a_1} + \frac{e_2}{\mu_0 a_2}}{\frac{e_1 e_2}{\mu_0^2 a_1 a_2}} \right) = \mu_0 N^2 \left( \frac{a_2 + a_1}{e_2 e_1} \right)$$

b)  $B_1 = \frac{\phi_1}{a_1} = \frac{NI}{R_{01} a_1} = \frac{NI \mu_0 a_1}{e_1 a_1} = \frac{\mu_0 NI}{e_1}$

$B_2 = \frac{\phi_2}{a_2} = \frac{NI}{R_{02} a_2} = \frac{\mu_0 NI}{e_2}$

3



$$\tilde{Z}_T = R + \frac{1}{\frac{1}{j\omega L + \frac{1}{j\omega C_1}} + \frac{1}{j\omega C_2}} = j\omega C_2$$

$$\tilde{Z}_T = R + \frac{1 - \omega^2 LC_1}{j\omega C_1 + j\omega C_2 (1 - \omega^2 LC_1)} = \frac{R + j(\omega^2 LC_1 - 1)}{j\omega(C_1 + C_2) - \omega^3 LC_1 C_2}$$

$\text{Re}(Z)$        $\text{Im}(Z)$

$$\tilde{I}(t) = \frac{V_0 e^{j\omega t}}{\tilde{Z}_T} = \frac{V_0 e^{j\omega t}}{|\tilde{Z}_T| e^{j\phi}} = \frac{V_0}{|\tilde{Z}_T|} e^{j(\omega t - \phi)} = \tilde{I}_0 e^{j\omega t} \text{ con } \tilde{I}_0 = \frac{V_0}{|\tilde{Z}_T|} e^{j(-\phi)}$$

$$\Rightarrow I(t) = \text{Re} \left\{ \frac{V_0}{|\tilde{Z}_T|} e^{j(\omega t - \phi)} \right\} = \frac{V_0}{|\tilde{Z}_T|} \cos(\omega t - \phi)$$

donde  $|\tilde{Z}_T| = \sqrt{\text{Re}^2(\tilde{Z}_T) + \text{Im}^2(\tilde{Z}_T)} = \sqrt{R^2 + \left( \frac{\omega^2 LC_1 - 1}{\omega(C_1 + C_2) - \omega^3 LC_1 C_2} \right)^2}$

y  $\phi = \text{arctg} \frac{\text{Im}(\tilde{Z}_T)}{\text{Re}(\tilde{Z}_T)} = \text{arctg} \left\{ \frac{\omega^2 LC_1 - 1}{R\omega[(C_1 + C_2) - \omega^2 LC_1 C_2]} \right\}$

$$\langle P \rangle = \frac{1}{2} \text{Re} \{ \tilde{V} \tilde{I}_0^* \} = \frac{1}{2} \text{Re} \left\{ V_0^2 \frac{e^{j\phi}}{|\tilde{Z}_T|} \right\} = \frac{1}{2} \frac{V_0^2 R}{R^2 + \left( \frac{\omega^2 LC_1 - 1}{\omega(C_1 + C_2) - \omega^3 LC_1 C_2} \right)^2}$$

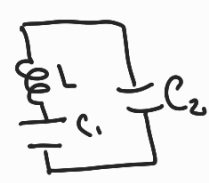
$\leftarrow \frac{1}{2} \frac{V_0^2}{|\tilde{Z}_T|} \cos\phi \frac{R}{|\tilde{Z}_T|} = \frac{1}{2} \frac{V_0^2 R}{|\tilde{Z}_T|^2}$

b)  $\omega_0$  tal que  $I_0(\omega_0) = I_{0\text{máx}}$ , la corriente máxima corresponde a  $|\tilde{Z}_T|$  mínimo y esto ocurre cuando la  $\text{Im}(\tilde{Z}_T) = 0$ :  $\omega^2 LC_1 - 1 = 0$

$$\Rightarrow \omega_0 = \frac{1}{\sqrt{LC_1}}$$

$\omega^*$  tal que  $I_0(\omega^*) = 0$ , la corriente por la resistencia se anula cuando  $|\tilde{Z}_T| \rightarrow \infty$ :  $(C_1 + C_2 - \omega^2 LC_1 C_2)\omega^* = 0 \rightarrow \omega^* = 0$  X

$$\omega^* = \frac{1}{\sqrt{L C_{\text{eq}}}} \text{ con } \frac{1}{C_{\text{eq}}} = \frac{1}{C_1} + \frac{1}{C_2} \text{ (serie)}$$



Se comporta como circuito  $L C_{\text{eq}}$  serie