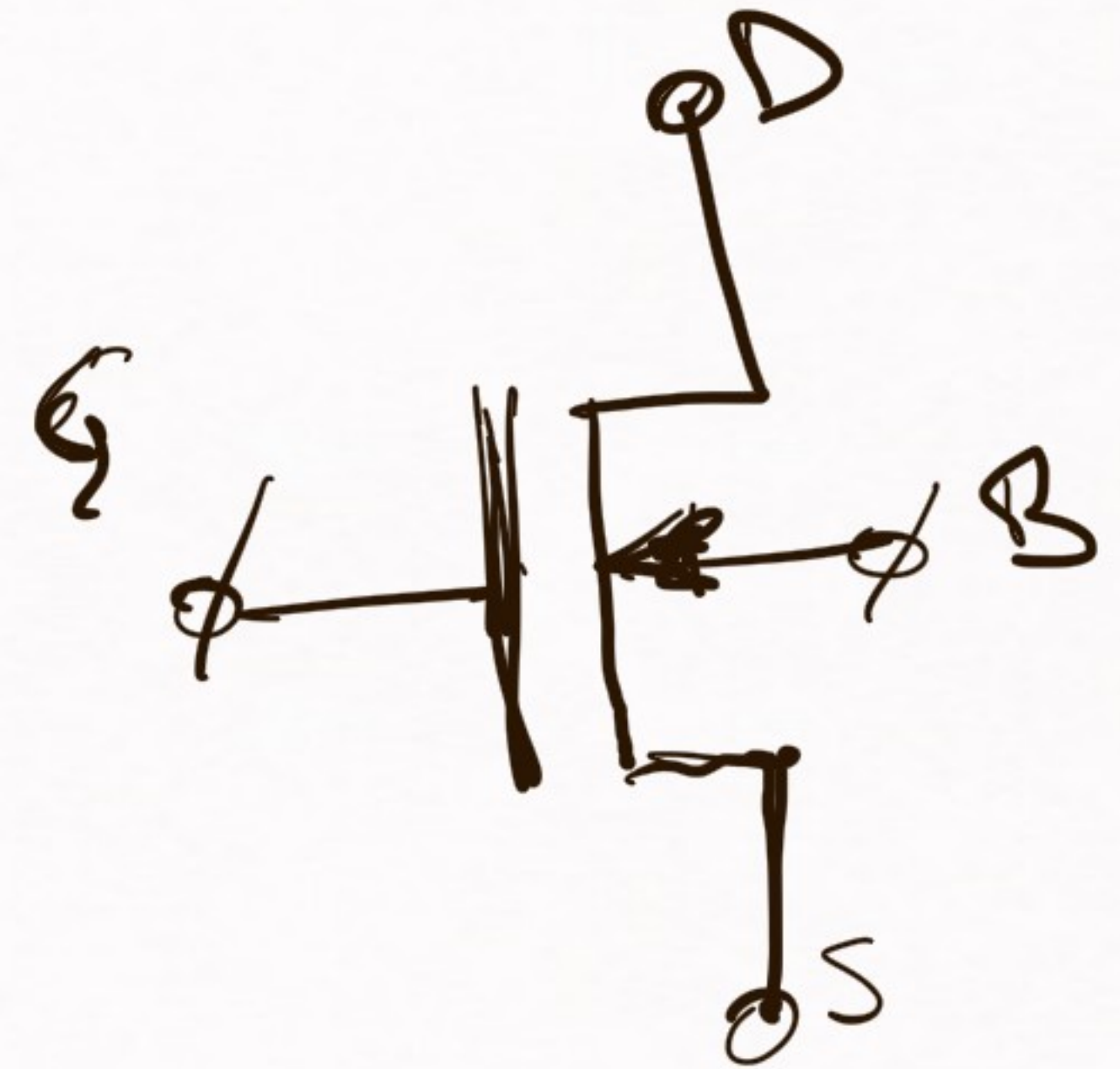
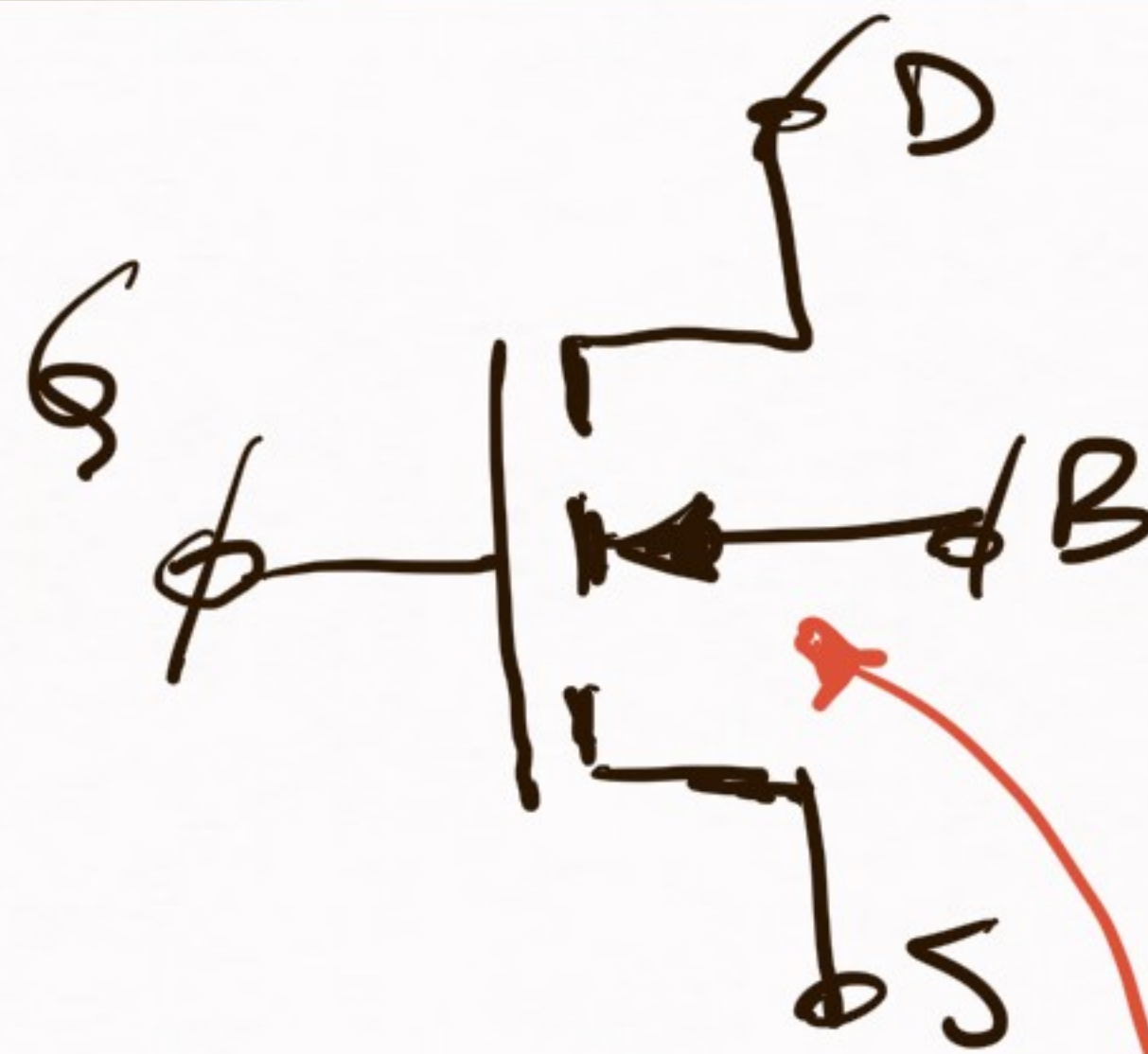
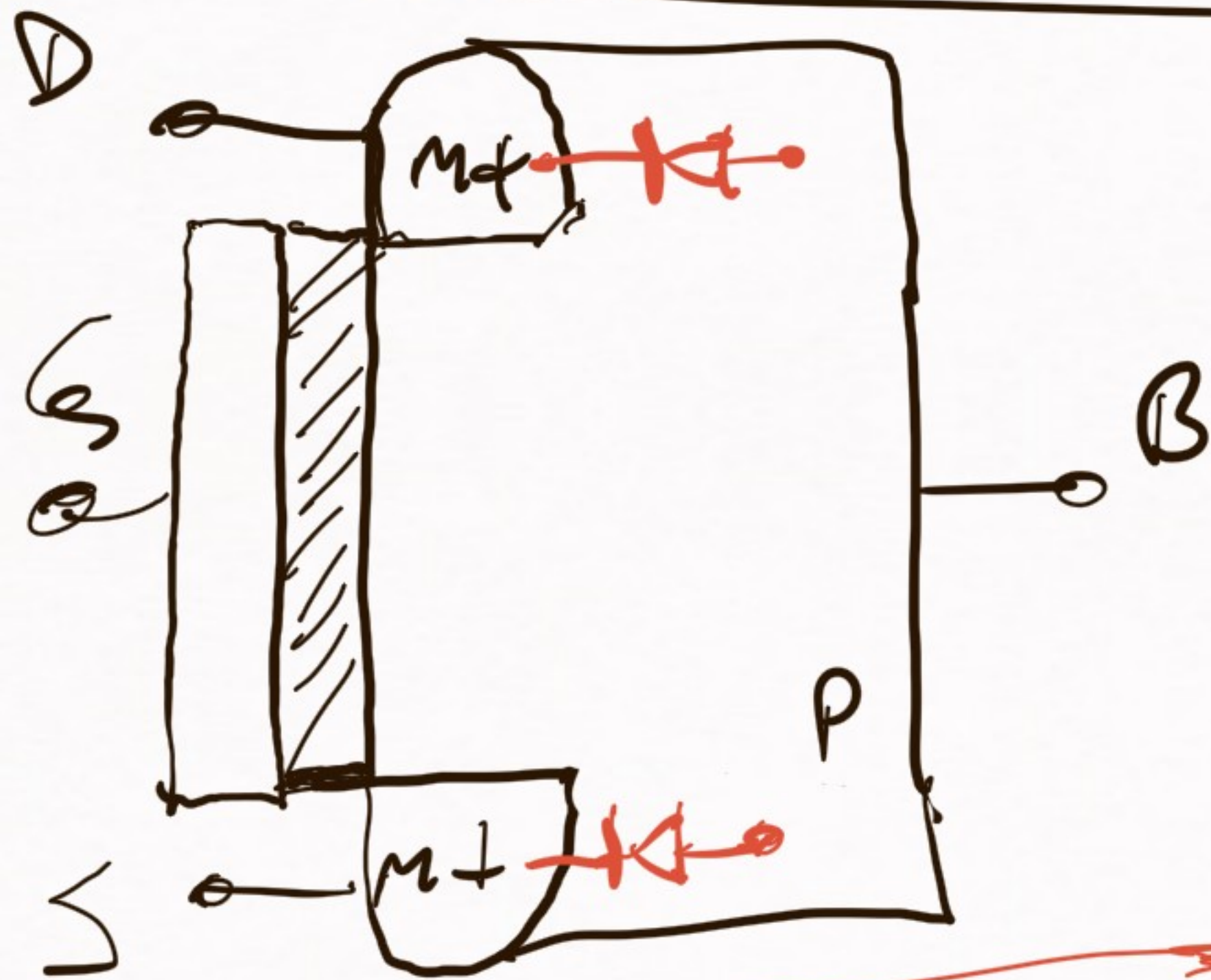


Simbolo de circuito del transistor MOS

21/4/2021

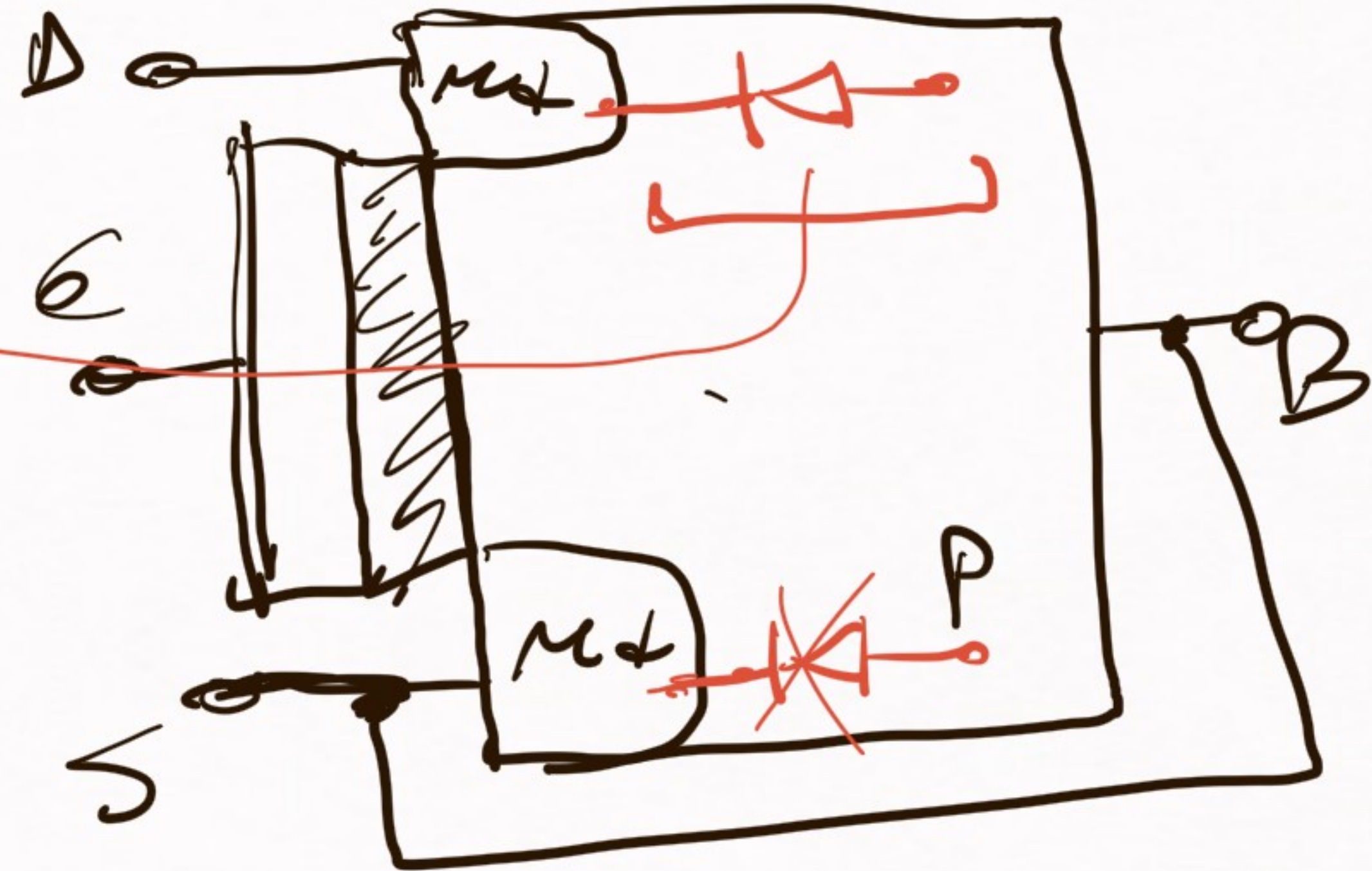
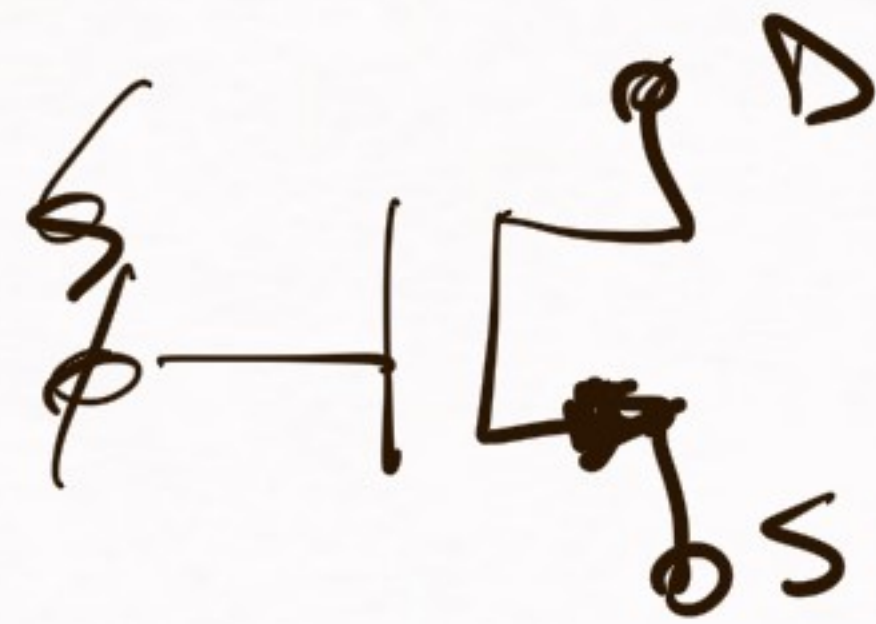
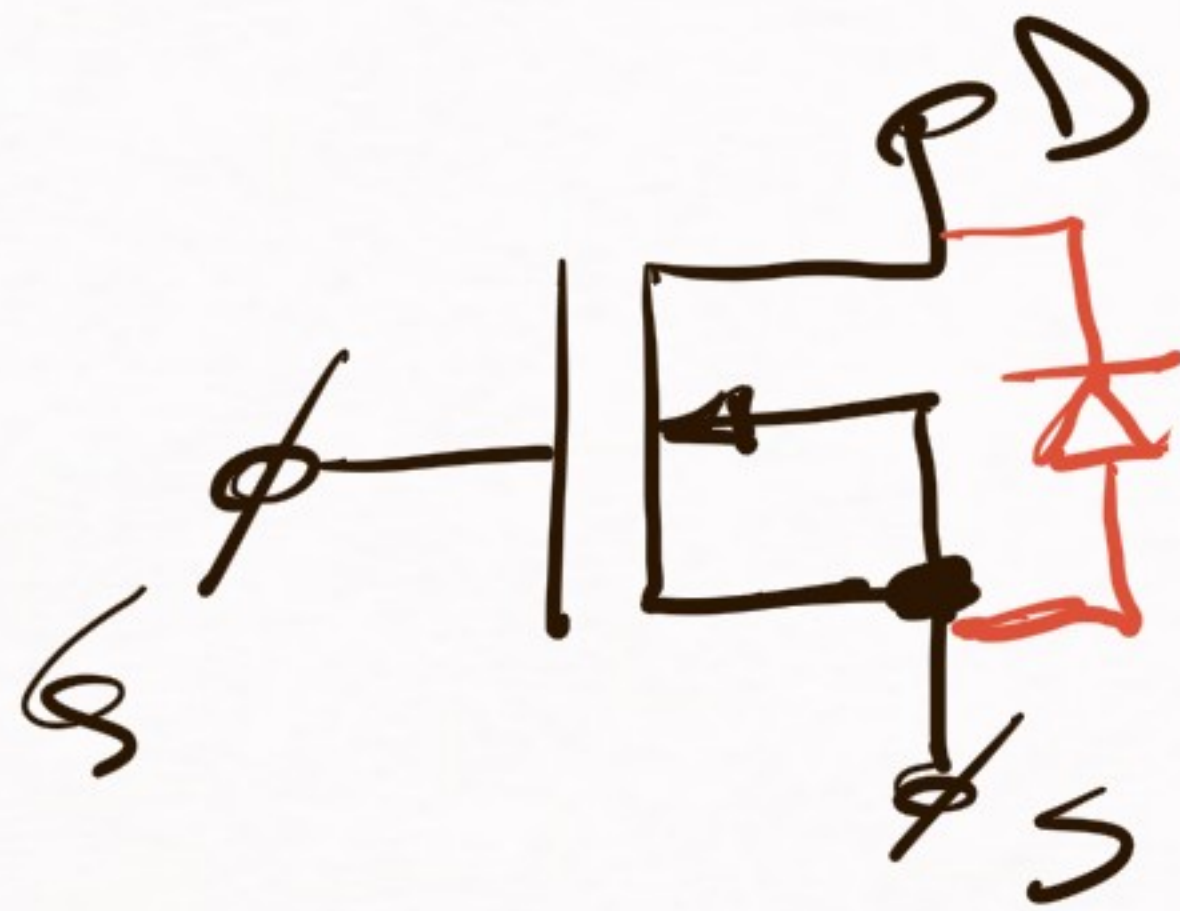


sin conexión
explícita de sustrato



flecha apunta en el
sentido directo de la
junctura B-S (o equiv. B-D)

Transistores MOS discretos



Transistor MOS discretos

- ↳ tienen 3 terminales
- ↳ No son simétricos respecto a S y D
- ↳ Tienen el diodo $D-B$ en "antiparalelo"

Ej. de análisis de circuitos con transistor MOS.

1) Uso como llave:

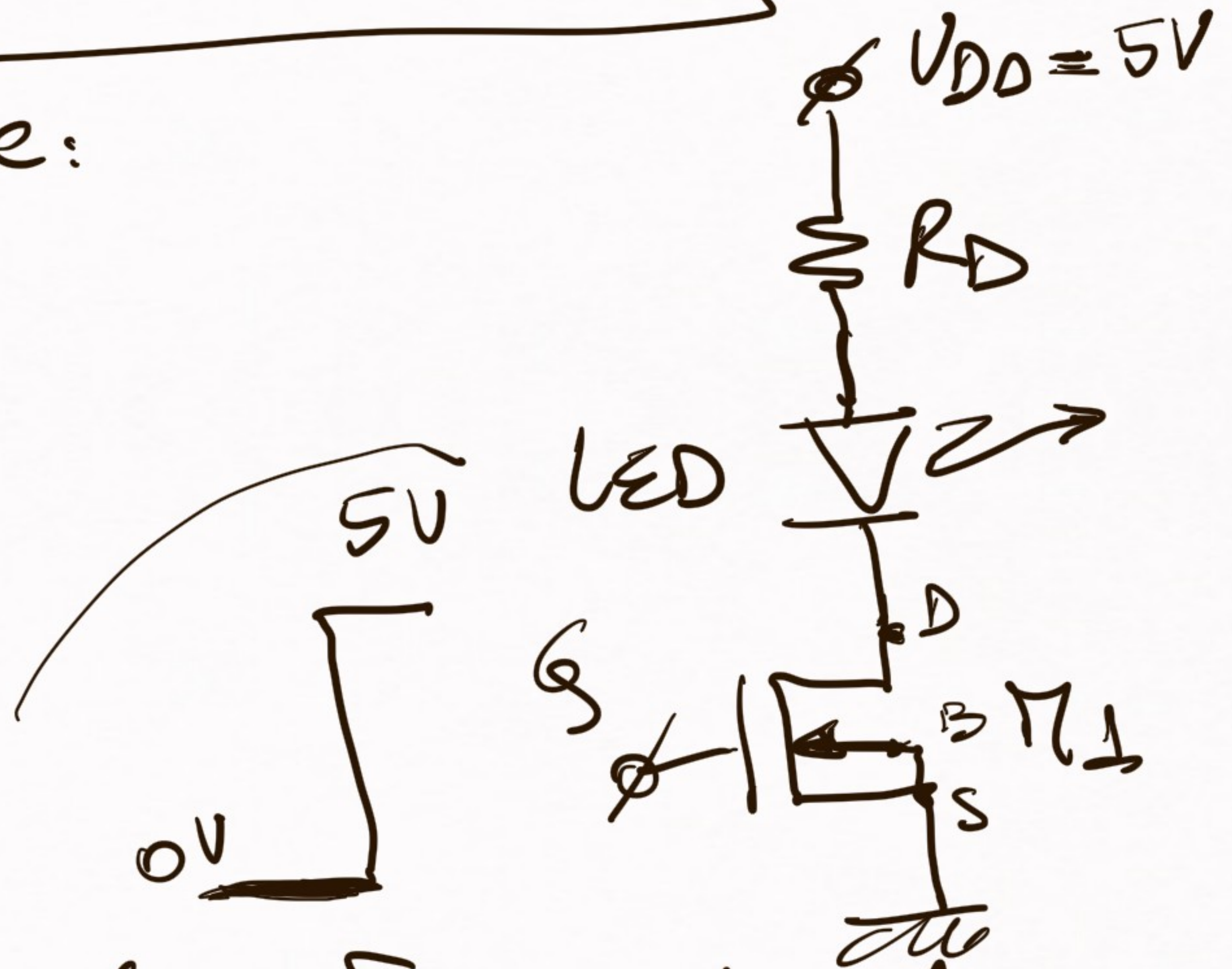
MOS: $V_{to} = 1.5V$

$f = 0.3$

$\beta = 0.1 A/V^2$

LED: $V_{LED} = 1.4V$

- Diseñar R_D para que $I_{LED} = 10mA$



1) $V_G = 0 \Rightarrow \textcircled{H}$ T1 cortado $\Rightarrow V_D = 0$
 $\Rightarrow I_{LED} = 0 \Rightarrow$ LED apagado

Verifico si la solución es
coherente con lo \textcircled{H} de T1
cortado:

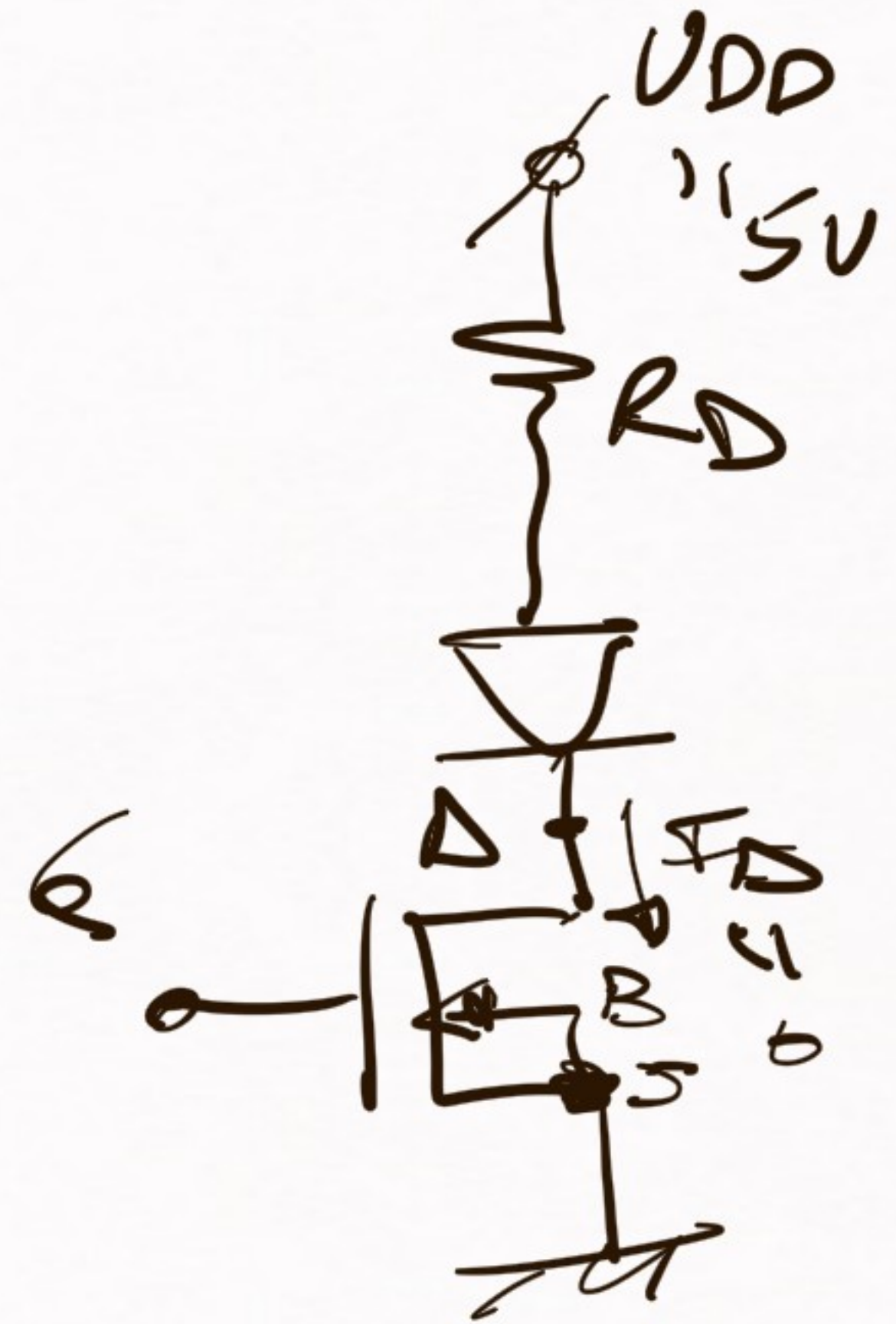
$$\left[V_S > V_P, \quad V_D (\geq V_S) > V_P \right]$$

$$V_S \stackrel{?}{>} V_P = \frac{V_G - V_{T0}}{(1+\beta)} = \frac{-1.5V}{1.3} \quad \checkmark$$

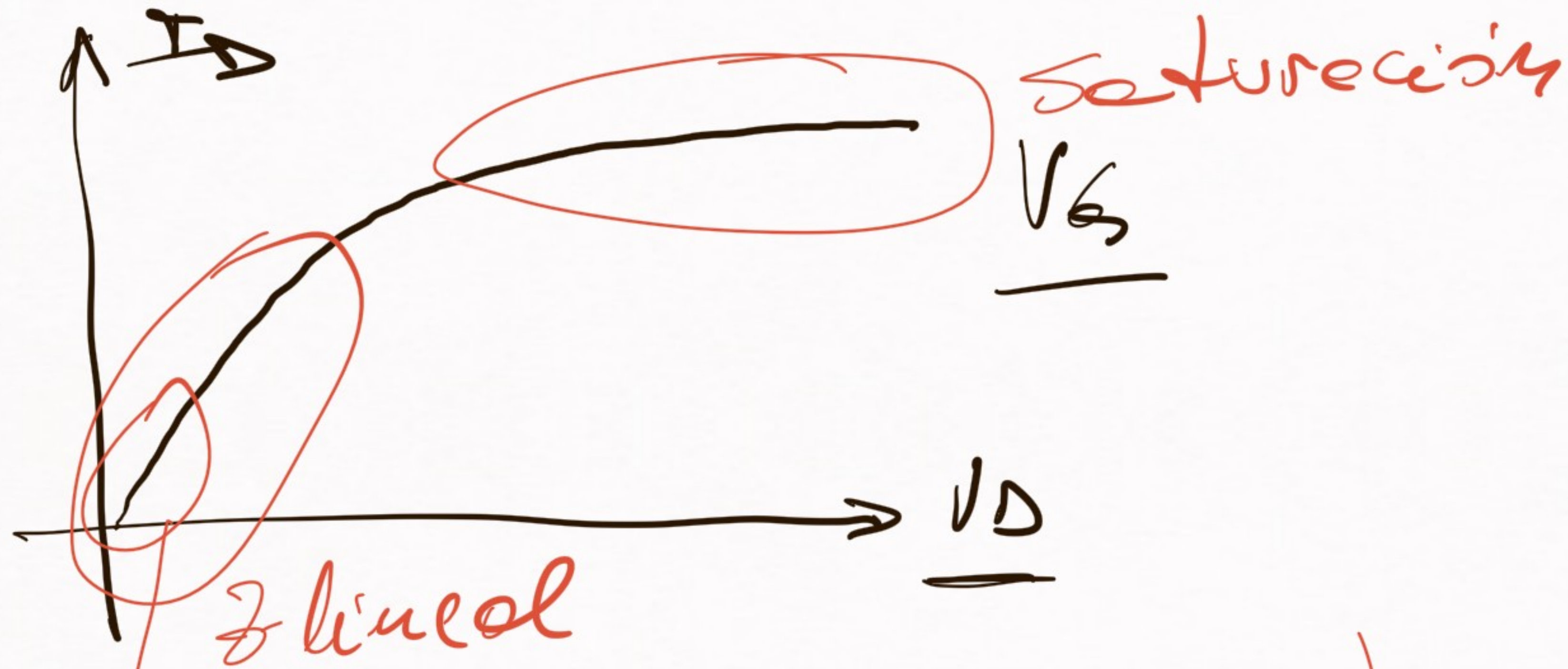
$$\begin{array}{c} V_{SB} \\ || \\ 0 \end{array}$$

$$V_D \stackrel{?}{>} V_P = \frac{-1.5V}{1.3}$$

$\rightarrow = 5V$

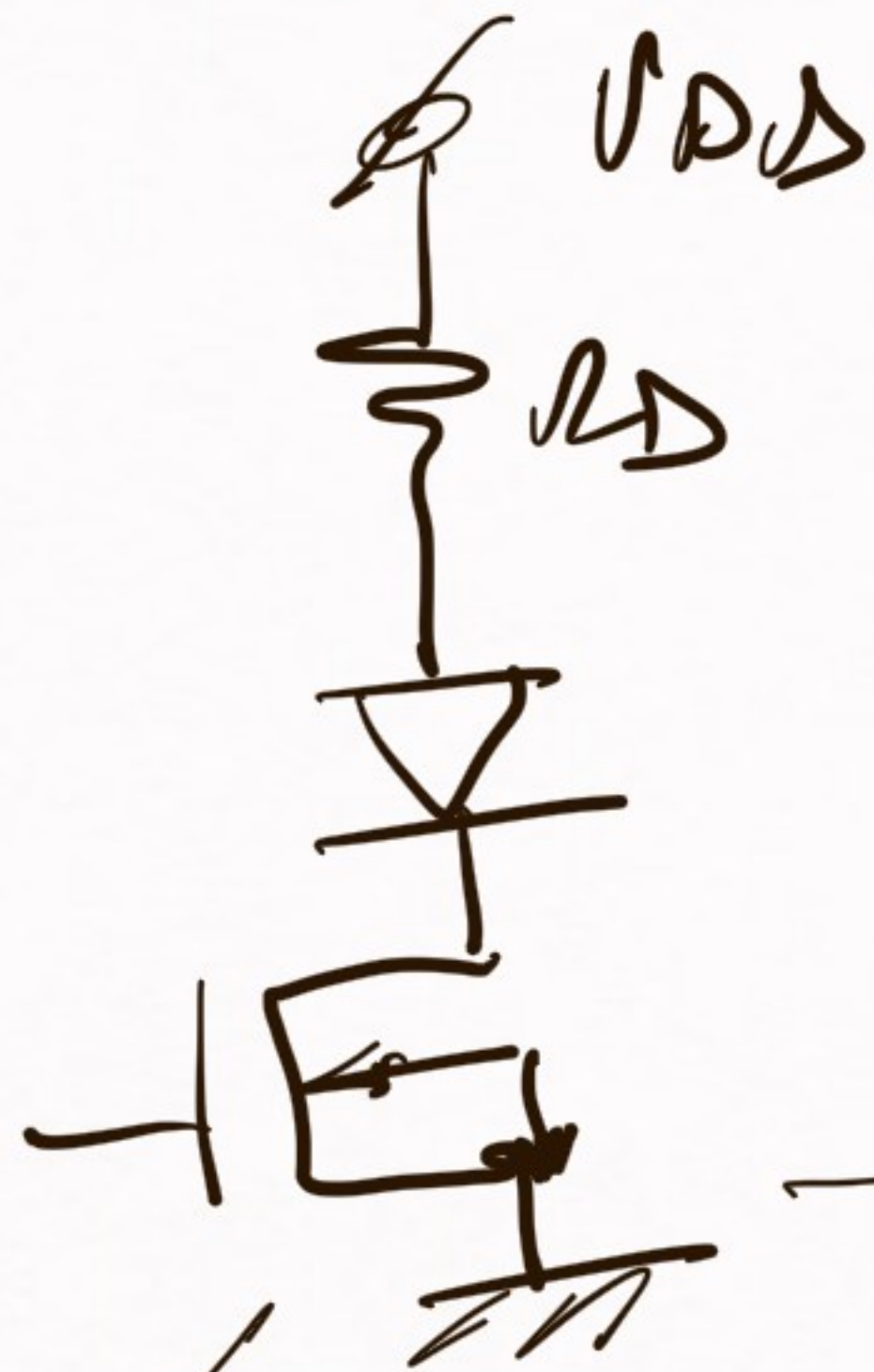


2) $V_G = 5V$



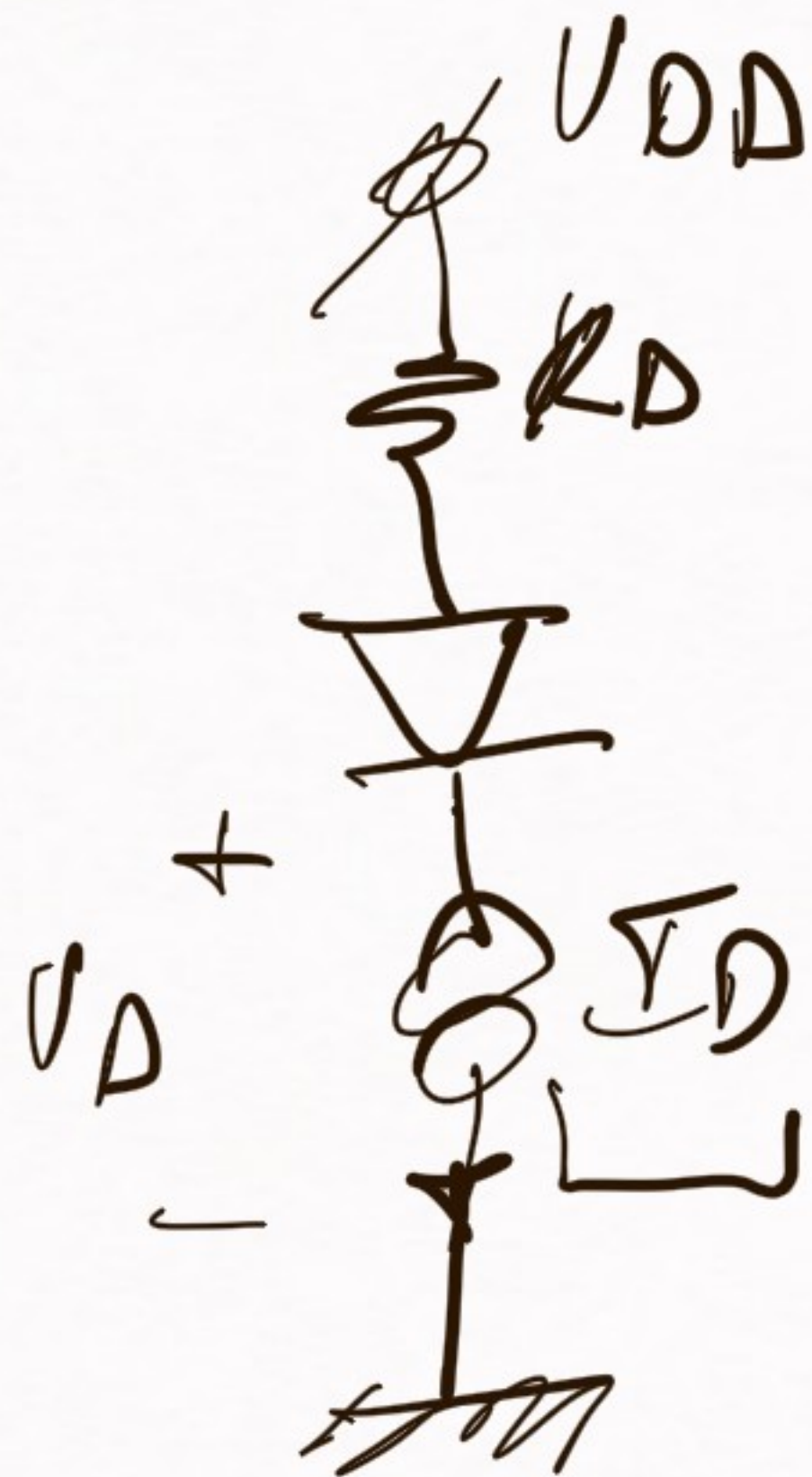
$\rightarrow I_{D1} \sim R_{ov}(V_G, V_{to}, \beta)$

π_1
sat.



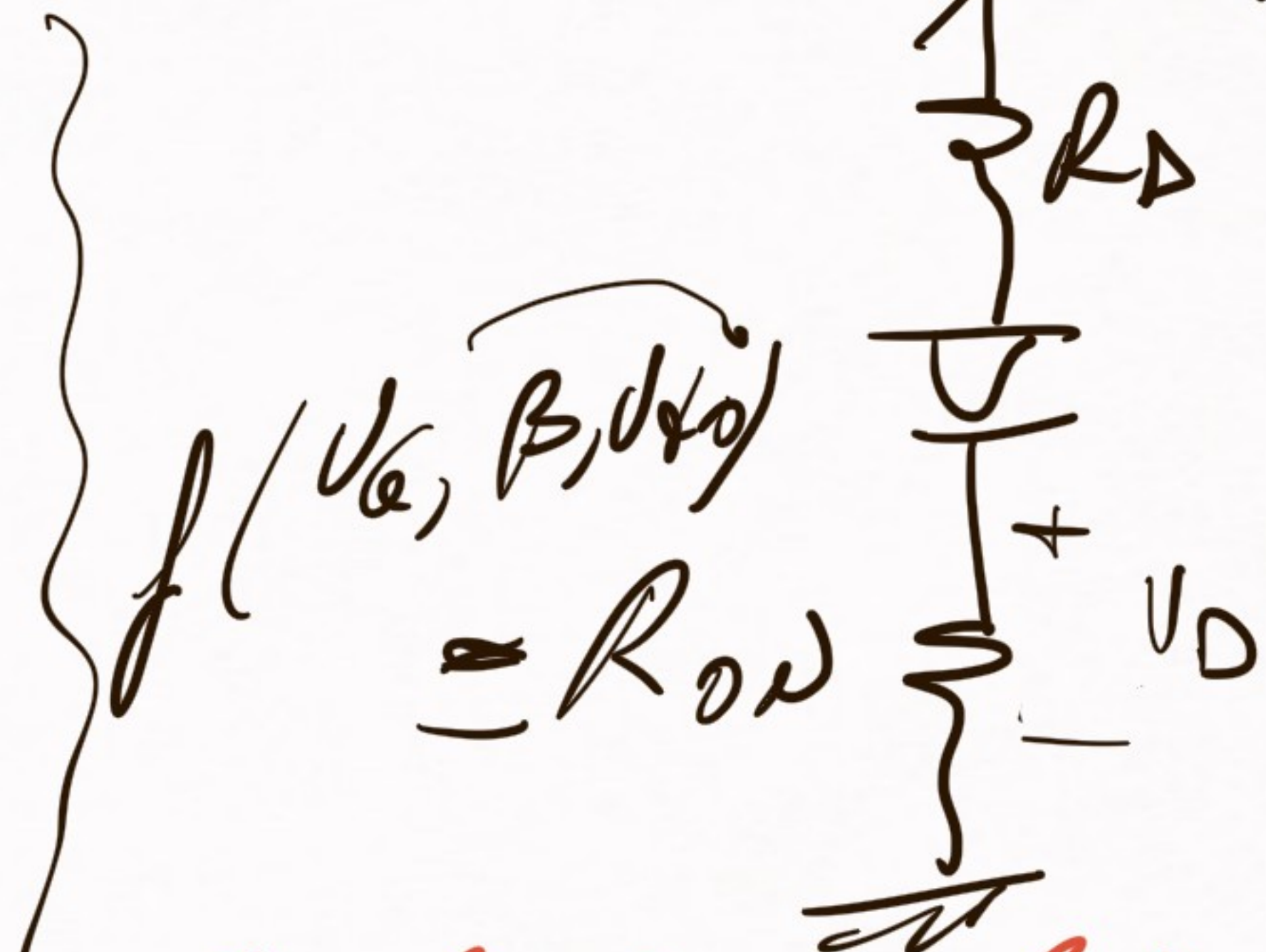
π_1 en 2.
lineal
($v_D \ll V_P$)

Ajustar V_G



$$i_D = f(V_G, V_{T0}, \beta, \epsilon)$$

dispersion

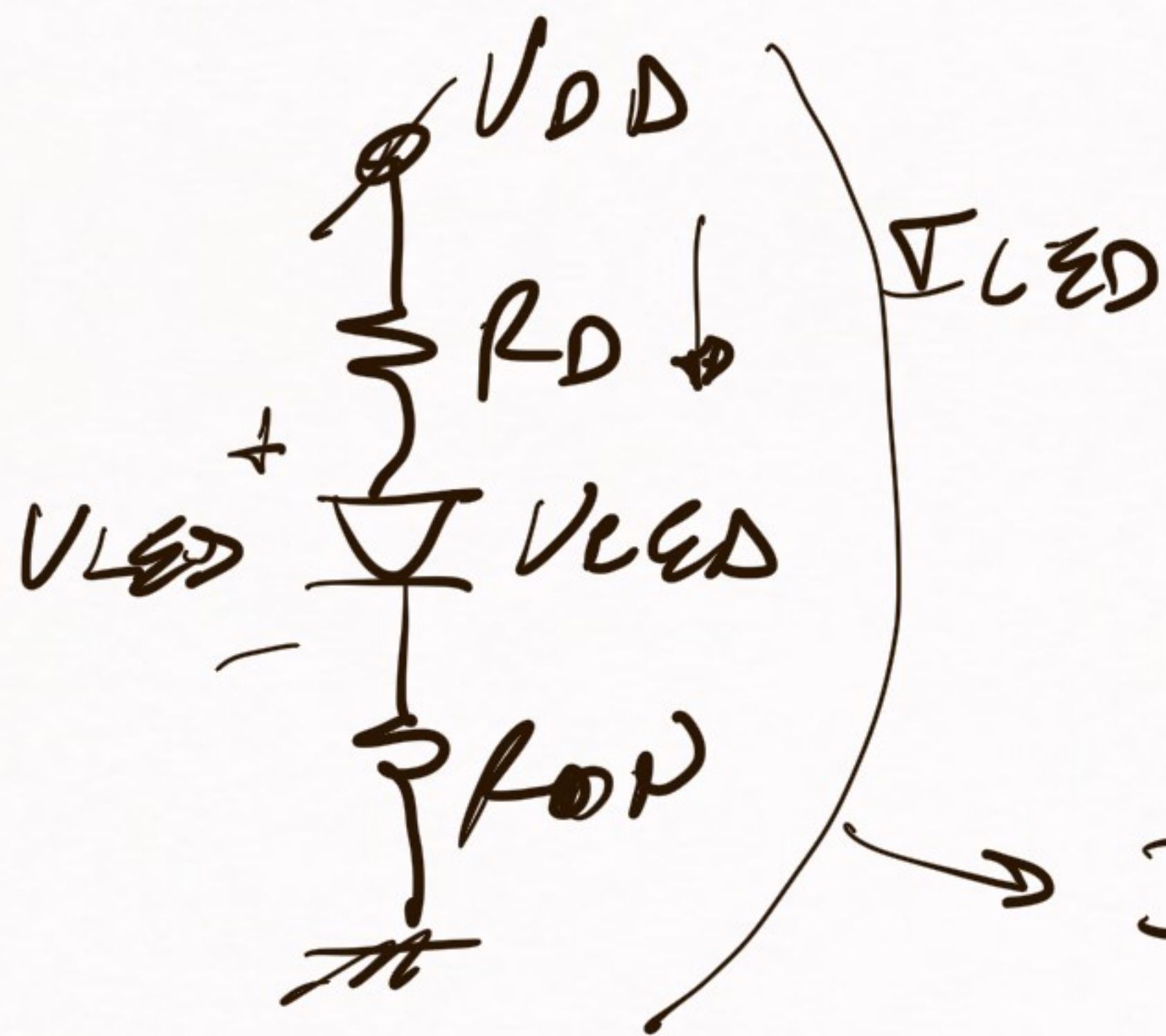


Si $R_{0D} \ll R_D$
 $\Rightarrow i_{RD}$ fijada por R_D

④ π 1 on zone lineal $\Rightarrow V_D / V_D \ll V_P$

$\begin{matrix} \nearrow \\ \rightarrow \end{matrix} V_S < V_P$
 $V_D < V_P$

π 1 \rightarrow R_{ON}



$$R_{ON} = \frac{1}{\beta(V_G - V_{th})} =$$

$$= \frac{1}{5 \cdot 0.1 \cdot (5 - 1.5)} = 2.9 \Omega$$

$$I_{LED} = \frac{V_{DD} - V_{LED}}{R_D + R_{ON}} \approx \frac{V_{DD} - V_{LED}}{R_D}$$

$\approx 20 \text{ mA}$

$R_{ON} \ll R_D$

$$\Rightarrow R_D + R_{ON} = 360 \Omega \Rightarrow R_D = 357 \Omega, R_D \approx 360 \Omega$$

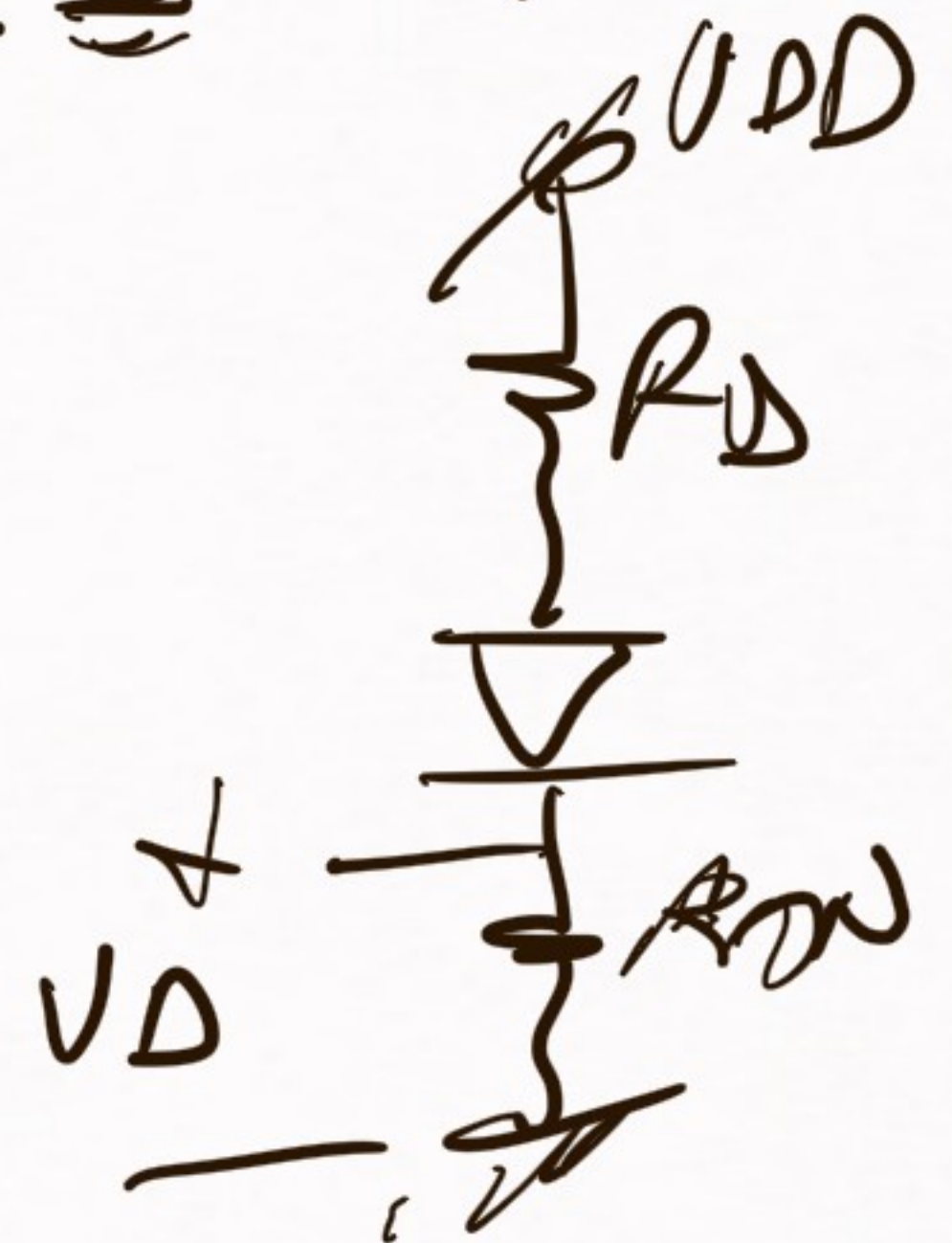
Verifica se: $V_S < V_P$

~~$(V_D < V_P)$~~ $\rightarrow V_D \ll V_P$

$V_S < V_P \Leftrightarrow V_G > \underbrace{V_{to}}_{1.5V} + \underbrace{(1+\beta)V_S}_{=0}$

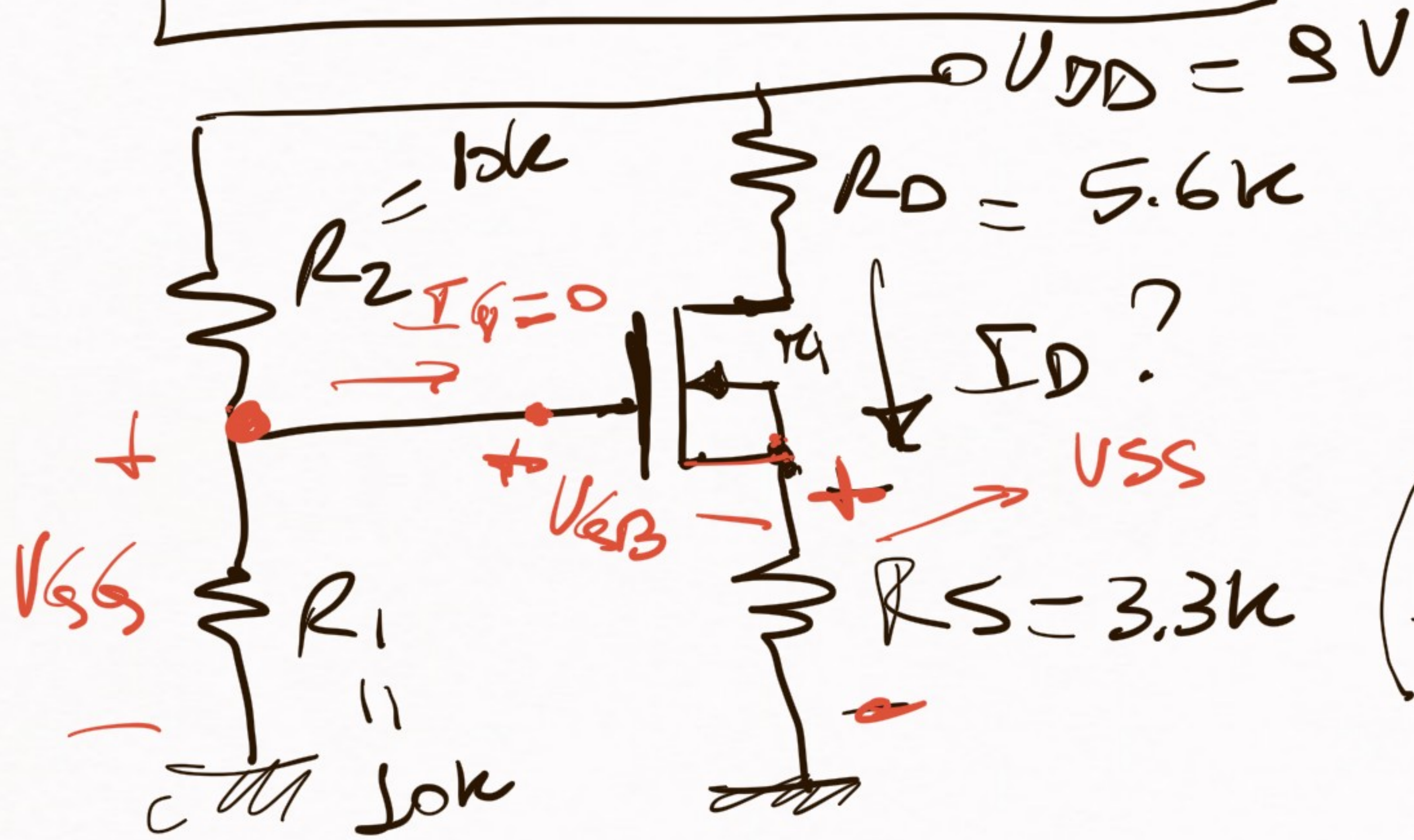
$V_D \ll V_P = \frac{V_G - V_{to}}{1+\beta} = \frac{5V - 1.5V}{1.3} = 2.7V$

$V_D = I_{ES} R_{ov} = I_{ov} \cdot 2.8\Omega =$
 29mV



$$\boxed{V_S < V_P} \iff \underbrace{V_G > V_{t0} + (1 + \delta) V_S}$$
$$\frac{V_G - V_{t0}}{(1 + \delta)}$$

Ej. en saturación:



$\mu_1: V_{to} = 1V$

$\beta = 1 \text{ mA/V}^2$
 $\gamma = 0$

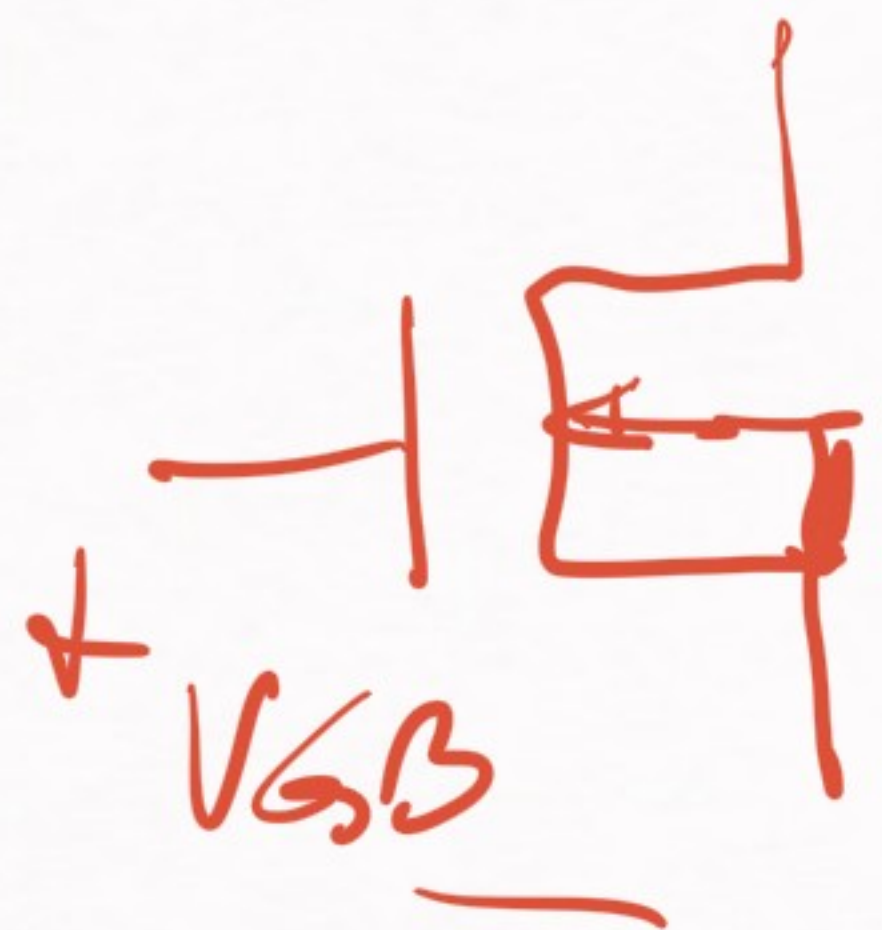
(K) μ_1 en saturación:

$$I_D = \frac{\beta}{2(1+\gamma)} (V_{GS} - V_{to} - \gamma V_{DS})^2$$

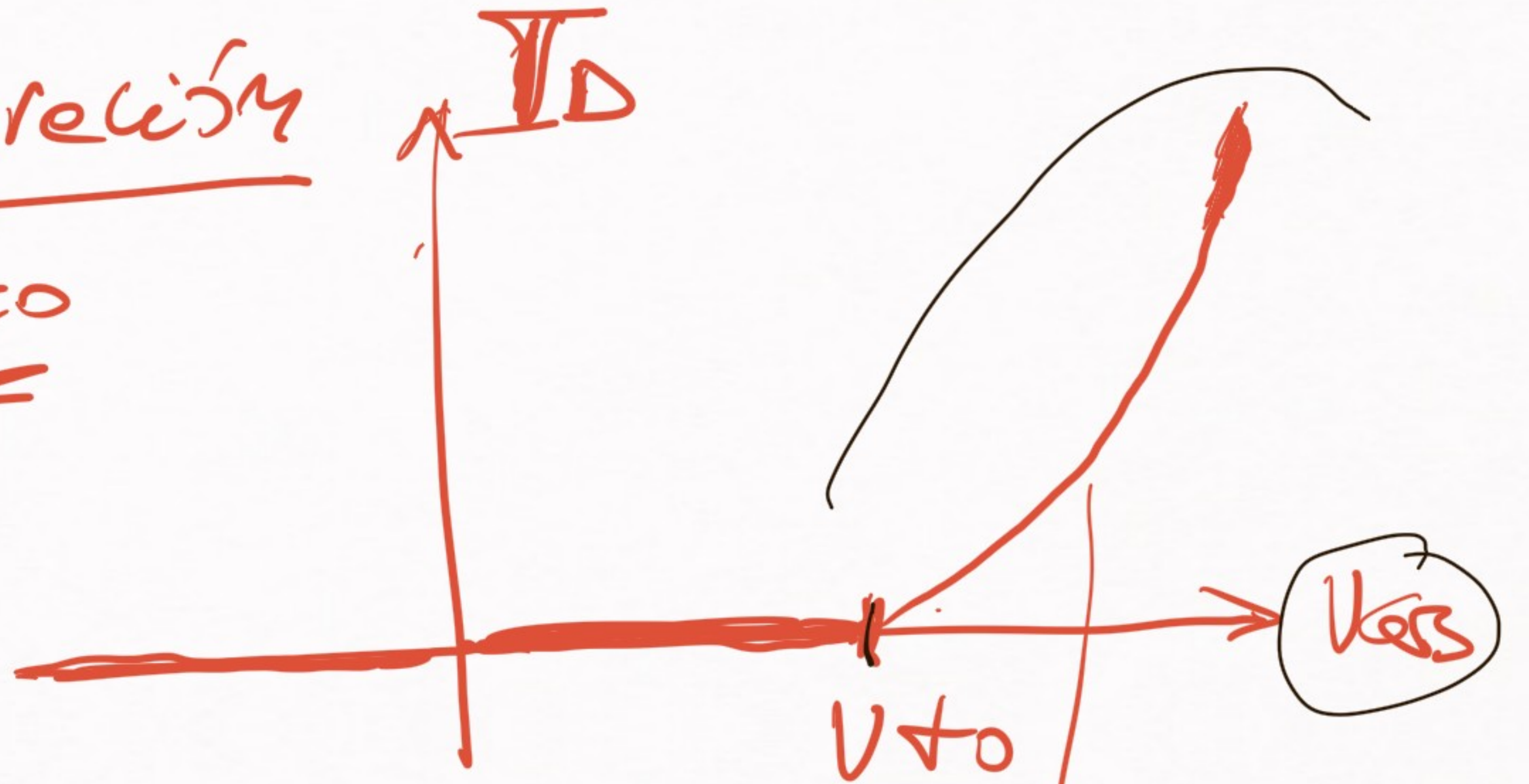
$$I_D = \frac{\beta}{2(1+\gamma)} (V_{GSB} - V_{to})^2$$

$$V_{GS} = \frac{R_2}{R_1 + R_2} V_{DD} = 4.5V$$

$$V_{SS} = I_D \cdot R_S \rightarrow V_{GSB} = V_{GS} - V_{SS} = V_{GS} - R_S \cdot I_D$$



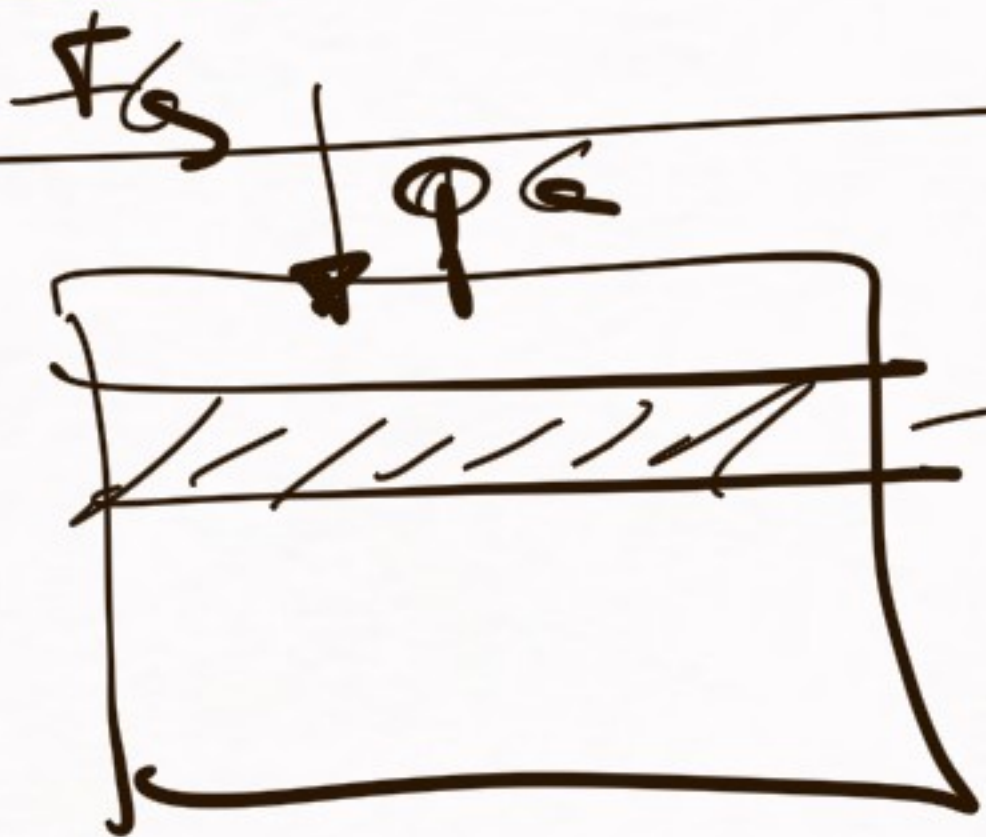
Saturación
 $V_{SD} = 0$



$$V_S < V_P \quad \frac{V_{GS} - V_{th}}{1 + f}$$

$V_{GS} > V_{th}$

$$I_D = \frac{\beta}{2(1+f)} (V_{GS} - V_{th})^2$$



→ en constante

$V_{GS,DC} = 0$

en continua

$$I_D = \frac{\beta}{2(1+\beta)} (V_{GS} - V_{th})^2$$

$$V_{GS} = V_{GS} - R_S \cdot I_D$$

$$V_{GS} = V_{GS} + R_S I_D = V_{GS} + \frac{R_S \beta (V_{GS} - V_{th})^2}{2(1+\beta)}$$

→ ec. de 2do grau em V_{GS}
 (o ec. de 2do grau em I_D)

$$\Rightarrow V_{GS} = \begin{cases} 2.18V \\ \cancel{0.79V} \end{cases}$$

no exemplo

$$V_S < V_P \Leftrightarrow V_{GS} > V_{th} + (1+\beta) V_S$$

$\underbrace{1V}_{IV} \quad \underbrace{0}_{0}$

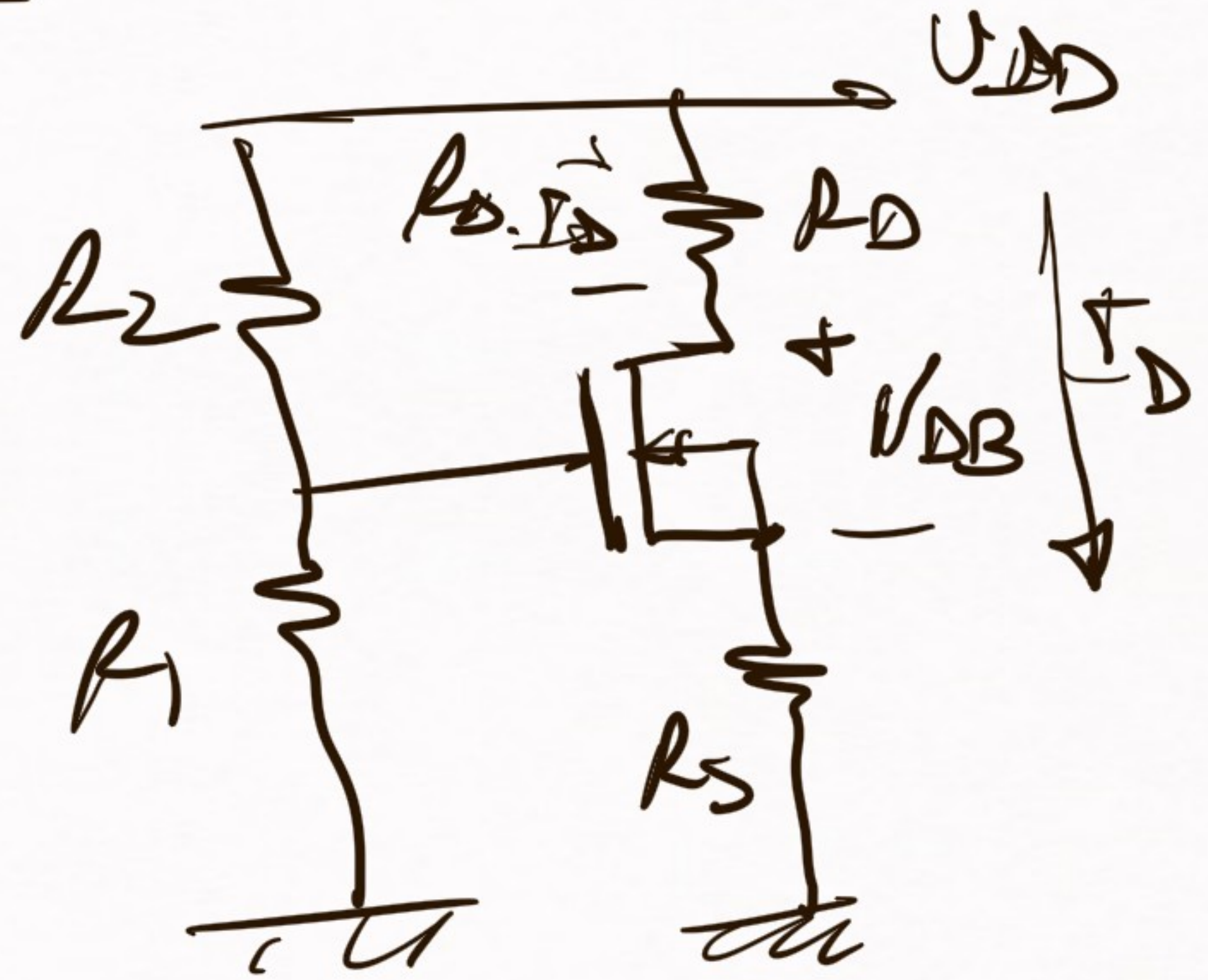
Saturation \Rightarrow

$$V_S < V_P \quad \checkmark$$

$$\underline{V_D > V_P}$$

$$V_D > V_P = \frac{V_{GS} - V_{th}}{(1 + \beta)}$$

$$= \frac{2.18 - 1}{1} = \underline{1.18V} \quad A$$



$$V_{DS} = V_{DD} - \underbrace{R_D \cdot I_D}_{= 3.32V} - \underbrace{R_S \cdot I_D}_{= 2.32V} = \underline{2.26V}$$

$$I_D = \frac{\beta}{2(1 + \beta)} (V_{GS} - V_{th})^2 = \frac{1e-3}{2 \cdot (1)} (2.18 - 1)^2 = 0.2 \mu A$$