

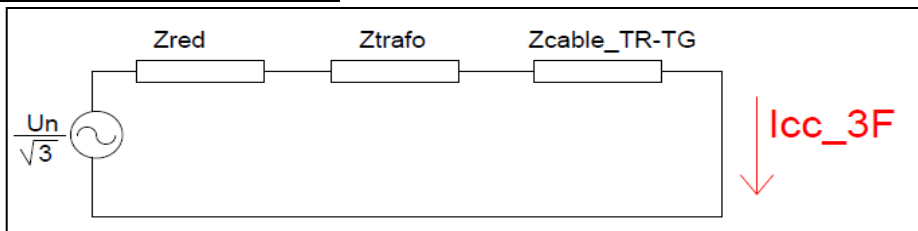
Solucion Examen DIC 2018

Parte (a)

Red: $S_{cc} = \text{inf.}$ \rightarrow $Z_{red}(\Omega) = 0$ $U_n(V): 400$

Trafo: $S_n(kVA): 1000$ \rightarrow $I_n(A): 1443$ $Z_{tr}(m\Omega): 1,92 + j7,76618310368742i$
 $u_{cc}(\%): 5\%$
 $|Z_{tr}| = u_{cc} \cdot U^2 / S_n = 8 \text{ m}\Omega$
 $P_{cu}(W) = 12000$
 $P_{cu} = 3 \cdot R_{tr} \cdot I_n^2 \rightarrow R_{tr} = 1,92 \text{ m}\Omega$
 $X_{tr} = \text{raiz}(|Z_{tr}|^2 - R_{tr}^2) = 7,77 \text{ m}\Omega$

Cable TR-TG: (3x240 por fase)
 $R_c = \rho \cdot L / S = 1,875 \text{ m}\Omega$ $Z_c(m\Omega): 0,625 + j0,5333333333333333i$
 $X_c = x_c \cdot L = 1,6 \text{ m}\Omega$



$Z_{equiv}(m\Omega) = 2,545 + j8,29951643702075i$ $I_{cc_3F}(kA) = U_n / \text{RAIZ}(3) / |Z_{equiv}| = 26,60$ \rightarrow **PdC > 26,60 kA**
 $|Z_{equiv}(m\Omega)| = 8,68095606$

Parte (b)

2 Motores de $P_n = 15 \text{ kW}$ \rightarrow $S(kVA) = 17,65$ \rightarrow $Q(kVAr) = 9,30$
 $\cos \phi = 0,85$
 $SL(kVA) = \text{raiz}[(P + 1,25 \cdot P)^2 + (Q + 1,25 \cdot Q)^2] = 39,71$ \rightarrow $I_L(A) = 57,3$

S(mm ²)	I(A)	Iz = I tabla x fa x ft (siendo fa x ft = 1)
10	52	X
16	67	OK \rightarrow S(mm²) = 16
25	86	OK
35	103	OK

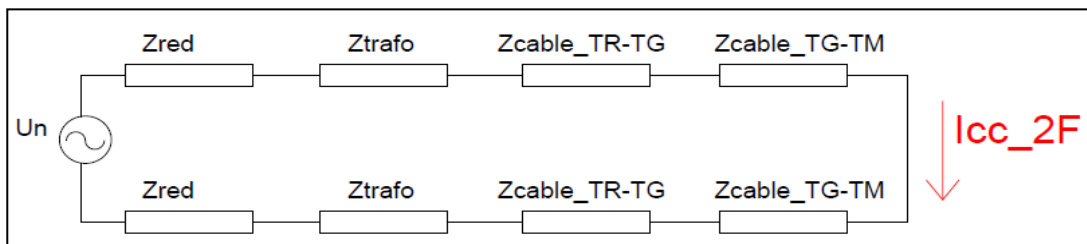
$\Delta U = \text{raiz}(3) \cdot I_d \cdot (R \cdot \cos \phi + X \cdot \text{sen} \phi) = 13,10 \text{ V}$ \rightarrow $\Delta U / U_n = 3,28\% < 4\%$

$I_d(A) = 50,9$
$R = \rho \cdot L / S = 0,17 \text{ }\Omega$
$X = x_c \cdot L = 0,0096 \text{ }\Omega$
$\cos \phi = 0,85$
$\text{sen} \phi = 0,53$

Parte (c)

$I_L < I_r < I_z \rightarrow 57,3A < I_r < 67A \rightarrow I_n = 63A \rightarrow I_m = 10 \times I_n = 630A$
 $PdC > I_{cc_max} \rightarrow PdC > 26,60kA \text{ (parte a)}$
 $(I^2 \times t) < (KS)^2 \rightarrow (I^2 \times t) < (115 \times 16)^2 = 3385600 \text{ A}^2 \cdot s$
 $I_m < I_{cc_min} \rightarrow I_m < 1,16kA$

Como el circuito entre el TG y T.Motores no tiene neutro, $I_{cc_min} = I_{cc_FF}$ en bornes del T.Motores:

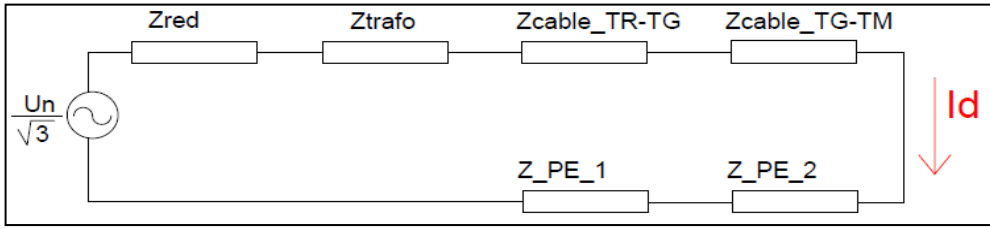


$Z_{red}(\Omega) = 0$
 $Z_{trafo}(m\Omega): 1,92 + j7,76618310368742i$ $Z_{equiv}(m\Omega) = Z_{red} + Z_{trafo} + Z_{c_TR-TG} + Z_{c_TG-TM} = 171,295 + j17,8995164370208i$
 $Z_{c_TR-TG}(m\Omega): 0,625 + j0,5333333333333333i$ $|Z_{equiv}(m\Omega)| = 172,2$
 $Z_{c_TG-TM}(m\Omega): 168,75 + j9,6i$ $I_{cc_2F} = U_n / (2 \cdot |Z_{equiv}|) = 1,16 \text{ kA}$

Parte (d)

HIP: $X_{PE} \approx 0 \Omega$

Se debe verificar que $I_m < I_d$ y que $t_{ap} < t_{max_seg} @ U_c$



$Z_{PE1} = \rho \cdot L / S1 =$	9	mΩ	$Z_{equiv}(m\Omega) = Z_{red} + Z_{trafo} + Z_{c_TR-TG} + Z_{c_TG-TM} + Z_{PE2} + Z_{PE1} =$	349,045 + 17,8995164370208i
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$Z_{PE2} = \rho \cdot L / S2 =$	168,75	mΩ	$ Z_{equiv}(m\Omega) =$	349,5
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$I_d = U_n / \sqrt{3} / |Z_{equiv}| = 661 \text{ A}$

$I_n = 63 \text{ A} \rightarrow I_m = 10 \times I_n = 630 \text{ A} \rightarrow$ Se verifica que $I_m < I_d$

Por otro lado, el tablero esta a la intemperie \rightarrow Local mojado

$U_c = Z_{pe} \cdot I_d = (Z_{pe1} + Z_{pe2}) \cdot I_d = 117,5 \text{ V} \rightarrow t_{max_seg} @ U_c = 117 \text{ V}: 0,18 \text{ s}$

Asumiendo que $t_{ap} < 180 \text{ ms}$, se puede concluir que el interruptor protege contra contactos indirectos.