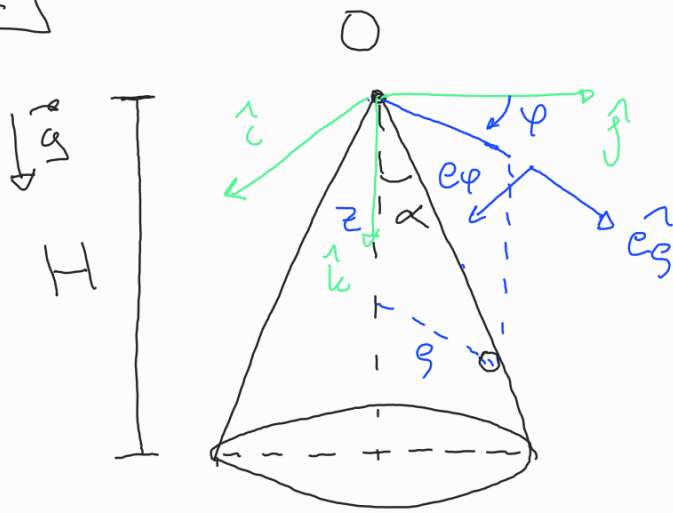


Examen Julio 2024. Mecánica Newtoniana

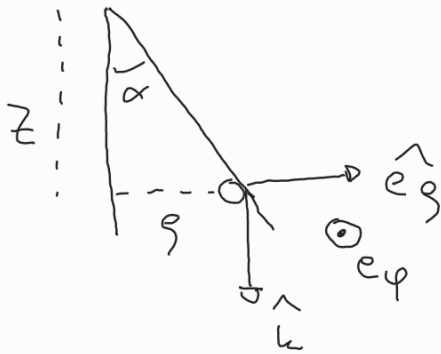
11



$\{\hat{e}_s, \hat{e}_\varphi, \hat{k}\}$ base de coordenadas similar a coordenadas cilíndricas

$\{\hat{z}, \hat{\rho}, \hat{k}\}$ sistema inercial

$$\vec{r} = \rho \hat{e}_s + z \hat{k}$$



$$\tan \alpha = \frac{\rho}{z} \Rightarrow \rho = z \tan \alpha$$

$$r = z \tan \alpha \hat{e}_s + z \hat{k}$$

$$\vec{v} = \dot{\rho} \hat{e}_s + \rho \dot{\varphi} \hat{e}_\varphi + \dot{z} \hat{k} \rightarrow \vec{v} = \dot{z} \tan \alpha \hat{e}_s + z \tan \alpha \dot{\varphi} \hat{e}_\varphi + \dot{z} \hat{k}$$

$$\vec{a} = (\ddot{z} \tan \alpha - z \tan \alpha \dot{\varphi}^2) \hat{e}_s + (z \tan \alpha \ddot{\varphi} + 2 \dot{z} \tan \alpha \dot{\varphi}) \hat{e}_\varphi + \ddot{z} \hat{k}$$

$$b) \frac{d(\vec{L}_O \cdot \hat{k})}{dt} = \frac{d\vec{L}_O}{dt} \cdot \hat{k} + \vec{L}_O \cdot \frac{d\hat{k}}{dt}$$

$$\frac{d(\vec{L}_O \cdot \hat{k})}{dt} = \frac{d\vec{L}_O}{dt} \cdot \hat{k}$$

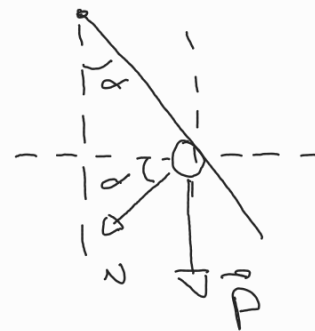
$$\vec{L}_O = (\vec{r} \wedge m \vec{v})$$

$$\frac{d\vec{L}_O}{dt} = \vec{v} \wedge m \vec{v} + \vec{r} \wedge m \vec{a}$$

Por 2^{da} Ley de Newton $\frac{d\vec{L}_O}{dt} = \vec{r} \wedge \vec{F}_N$

$$\vec{F}_N = mg \hat{k} - N \cos \alpha \hat{e}_g + N \sin \alpha \hat{k}$$

$$\vec{F}_z = (mg + N \sin \alpha) \hat{k} - N \cos \alpha \hat{e}_g$$



$$\frac{d\vec{L}_O}{dt} = (z \operatorname{tg} \alpha \hat{e}_g + z \hat{k}) \wedge ((mg + N \sin \alpha) \hat{k} - N \cos \alpha \hat{e}_g)$$

$$= (mg + N \sin \alpha) (z \operatorname{tg} \alpha) (-\hat{e}_\varphi) + z N \cos \alpha (-\hat{e}_\varphi)$$

$$= \left[(mg + N \sin \alpha) z \operatorname{tg} \alpha + N z \cos \alpha \right] (-\hat{e}_\varphi)$$

$$\Rightarrow \frac{d\vec{L}_O \cdot \hat{k}}{dt} = 0 \quad \text{pues } \hat{k} \cdot \hat{e}_\varphi = 0$$

$$\hookrightarrow \frac{d(\vec{L}_O \cdot \hat{k})}{dt} = 0 \quad \vec{L}_O \cdot \hat{k} \text{ constante}$$

$$\begin{aligned} c) \quad \vec{P}_N &= \vec{N} \cdot \vec{v} = (N \sin \alpha \hat{k} - N \cos \alpha \hat{e}_g) \cdot (\dot{z} \operatorname{tg} \alpha \hat{e}_g + z \operatorname{tg} \alpha \dot{\varphi} \hat{e}_\varphi + \dot{z} \hat{k}) \\ &= -N \cos \alpha \dot{z} \operatorname{tg} \alpha + N \sin \alpha \dot{z} = 0 \end{aligned}$$

$$\hookrightarrow \operatorname{tg} \alpha = \frac{\sin \alpha}{\cos \alpha}$$

El sistema es conservativo.

$$E = T + U \quad T = \frac{1}{2} m \vec{v}^2$$

$$U_g = -mgz \quad T = \frac{1}{2} m (\dot{z} \operatorname{tg} \alpha \hat{e}_g + z \dot{\varphi} \operatorname{tg} \alpha \hat{e}_\varphi + \dot{z} \hat{k})^2$$

$$T = \frac{1}{2} m (\dot{z}^2 (1 + \operatorname{tg}^2 \alpha) + z^2 \dot{\varphi}^2 \operatorname{tg}^2 \alpha)$$

$$\begin{aligned} \vec{L}_O &= (z \operatorname{tg} \alpha \hat{e}_g + z \hat{k}) \wedge m (\dot{z} \operatorname{tg} \alpha \hat{e}_g + z \dot{\varphi} \operatorname{tg} \alpha \hat{e}_\varphi + \dot{z} \hat{k}) \\ &= m z^2 \operatorname{tg}^2 \alpha \dot{\varphi} \hat{k} + m z \operatorname{tg} \alpha \dot{z} (-\hat{e}_\varphi) + m z \dot{z} \operatorname{tg} \alpha \hat{e}_\varphi - m z^2 \dot{\varphi} \operatorname{tg} \alpha \hat{e}_g \end{aligned}$$

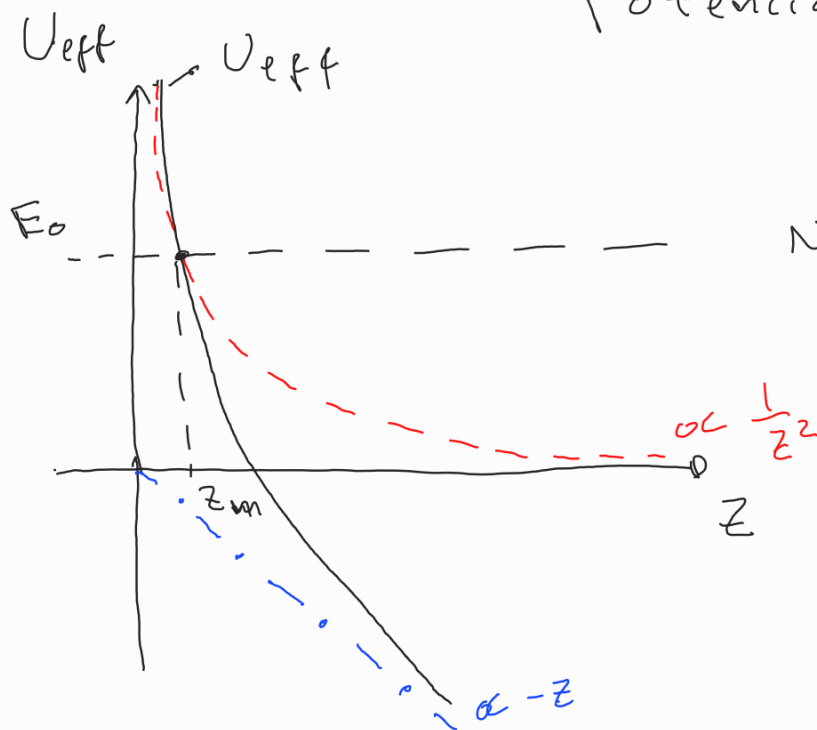
$$\vec{L}_0 \cdot \hat{k} = m \dot{z}^2 \tan^2 \alpha \dot{\varphi} = l_0 \text{ cte} \Rightarrow \dot{\varphi} = \frac{l_0}{m \dot{z}^2 \tan^2 \alpha}$$

$$T = \frac{1}{2} m \left(\dot{z}^2 (1 + \tan^2 \alpha) + \frac{l_0^2}{m^2 \dot{z}^4 \tan^4 \alpha} \right)$$

$$= \frac{1}{2} m \dot{z}^2 (1 + \tan^2 \alpha) + \frac{l_0^2}{2m \tan^2 \alpha} \frac{1}{\dot{z}^2}$$

$$E_0 = \frac{1}{2} m \dot{z}^2 (1 + \tan^2 \alpha) + \frac{l_0^2}{2m \tan^2 \alpha} \frac{1}{\dot{z}^2} - mgz \text{ cte.}$$

Potencial Efectivo
 $U_{\text{eff}}(z)$



No es posible tener
órbitas de altura
constante ya que
 $\forall E_0$ No hay
soluciones con \dot{z} cte.

Otra forma: las soluciones de altura constante z_0
ocurren si $\left. \frac{dU_{\text{eff}}}{dz} \right|_{z_0} = 0$

$$\frac{dU_{\text{eff}}}{dz} = -\frac{l_0^2}{2m \tan^2 \alpha} \frac{2}{z^3} - mg \stackrel{?}{=} 0 \Rightarrow z^3 = -\frac{l_0^2}{2mg \tan^2 \alpha}$$

resultado absurdo pues $z > 0$

d) si en $t=0$ $z(0) = \frac{H}{2}$ y $\vec{v}(0) = v_0 \hat{e}_\varphi$ la velocidad es horizontal y tangente al cono
 $\dot{z}(0) = 0$

$$\vec{v} = \dot{z} \operatorname{tg} \alpha \hat{e}_z + z \dot{\varphi} \hat{e}_\varphi + \dot{z} \hat{k}$$

$$\vec{v}(0) = \frac{H}{2} \dot{\varphi}_0 \operatorname{tg} \alpha \hat{e}_\varphi = v_0 \hat{e}_\varphi \Rightarrow \dot{\varphi}_0 = \frac{2v_0}{H \operatorname{tg} \alpha}$$

$$l_0 = m z_0^2 \operatorname{tg}^2 \alpha \dot{\varphi}_0 = m \frac{H}{2} \operatorname{tg} \alpha v_0$$

$$l_0 = \frac{m H}{2} \operatorname{tg} \alpha v_0$$

$$\vec{F}_N = (mg + N \sin \alpha) \hat{k} - N \cos \alpha \hat{e}_z$$

2^{da} Ley de Newton según \hat{k} $m \ddot{z} = mg + N \sin \alpha$

Según \hat{e}_z) $m (\ddot{z} \operatorname{tg} \alpha - z \operatorname{tg} \alpha \dot{\varphi}^2) = -N \cos \alpha$

$$mg \operatorname{tg} \alpha + N \operatorname{tg} \alpha \sin \alpha - m z \operatorname{tg} \alpha \frac{l_0^2}{m^2 z^4 \operatorname{tg}^4 \alpha} = -N \cos \alpha$$

$$\dot{\varphi} = \frac{l_0}{m z^2 \operatorname{tg} \alpha}$$

$$\rightarrow mg \operatorname{tg} \alpha - m \operatorname{tg} \alpha \frac{\left(\frac{m H}{2} \operatorname{tg} \alpha v_0\right)^2}{m^2 \operatorname{tg}^4 \alpha} \frac{1}{z^3} = -N \left(\cos \alpha + \frac{\sin^2 \alpha}{\cos \alpha} \right)$$

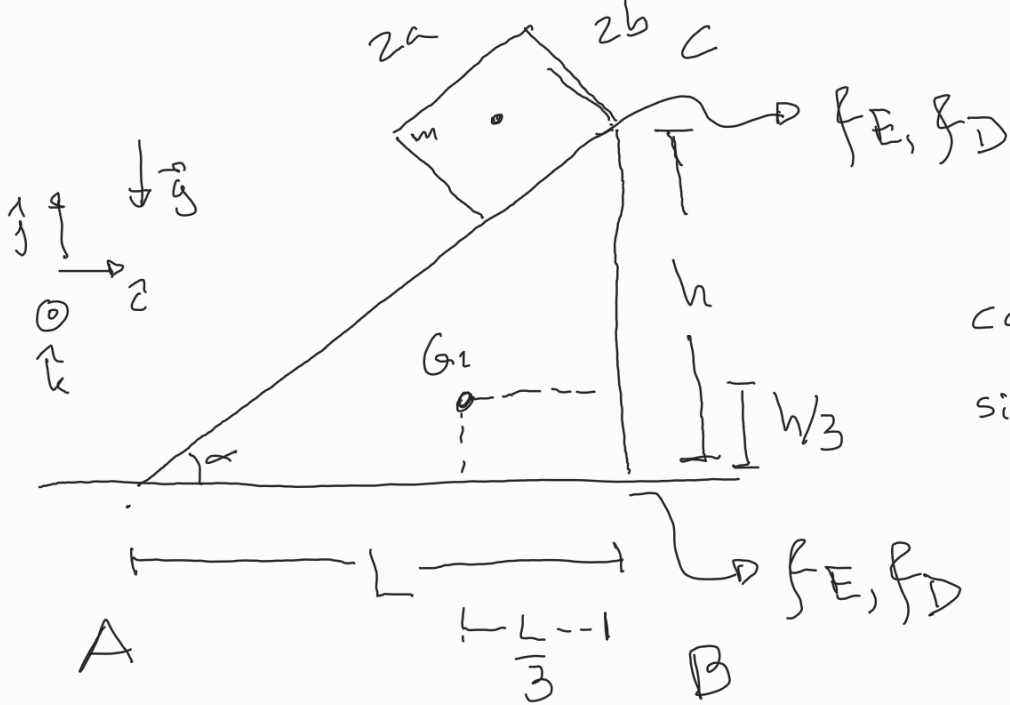
En $z=H$

$$mg \operatorname{tg} \alpha - m \frac{v_0^2}{4H \operatorname{tg} \alpha} = -\frac{N}{\cos \alpha} \rightarrow N > 0 \Leftrightarrow m \left(\frac{v_0^2}{4H \operatorname{tg} \alpha} - g \operatorname{tg} \alpha \right) > 0$$

$$\Rightarrow v_0^2 \geq 4H g \operatorname{tg}^2 \alpha$$

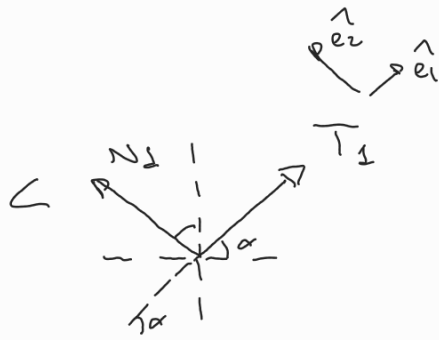
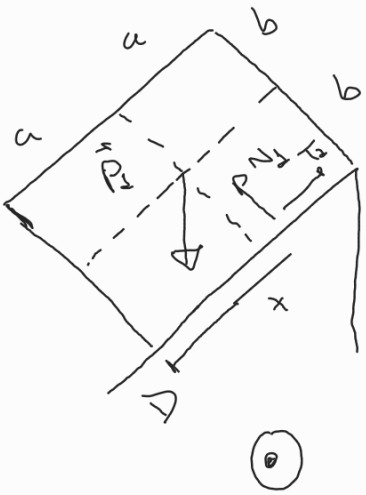
$$v_0 = 2 \sqrt{H g} \operatorname{tg} \alpha$$

2



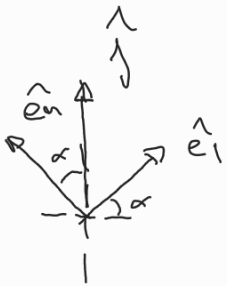
$$\cos \alpha = \frac{\sqrt{3}}{2}$$

$$\sin \alpha = \frac{1}{2}$$



$$\vec{T}_\perp = T_\perp \cos \alpha \hat{z} + T_\perp \sin \alpha \hat{y}$$

$$\vec{N}_\perp = -N_\perp \sin \alpha \hat{z} + N_\perp \cos \alpha \hat{y}$$



$$\hat{z}) \quad T_\perp \cos \alpha = N_\perp \sin \alpha$$

$$\hat{y}) \quad T_\perp \sin \alpha + N_\perp \cos \alpha = mg$$

$$\hat{y} = \cos \alpha \hat{e}_n + \sin \alpha \hat{e}_t$$

Momentos nulos: $\vec{M}_D = 0$

$$0 = N_\perp x \hat{y} - mg \cos \alpha a \hat{y} + mg b \sin \alpha \hat{y}$$

$$N_\perp x = mg(a \cos \alpha - b \sin \alpha)$$

$$T_{\perp} \frac{\sqrt{3}}{2} = N_{\perp} \frac{1}{2} \rightarrow T_{\perp} = \frac{1}{\sqrt{3}} N_{\perp} \quad \vee \quad \frac{1}{2} \frac{1}{\sqrt{3}} N_{\perp} + \frac{\sqrt{3}}{2} N_{\perp} = mg$$

$$4 N_{\perp} = 2\sqrt{3} mg \rightarrow \boxed{N_{\perp} = \frac{\sqrt{3}}{2} mg} \quad \left| \quad \boxed{T_{\perp} = \frac{1}{2} mg} \right.$$

$$\frac{\sqrt{3}}{2} mg x = mg \left(a \frac{\sqrt{3}}{2} - \frac{b}{2} \right) \rightarrow \boxed{x = a - \frac{b}{\sqrt{3}}}$$

Condiciones: $N_{\perp} \geq 0$ se cumple

$$|\vec{T}_{\perp}| \leq f_E |\vec{N}_{\perp}| \rightarrow \frac{1}{2} mg \leq f_E \frac{\sqrt{3}}{2} mg$$

$$\boxed{f_E \geq \frac{1}{\sqrt{3}}}$$

Si no se cumple la placa desliza hacia abajo

$$0 \leq x \leq 2a \rightarrow 0 \leq x \Rightarrow a > \frac{b}{\sqrt{3}} \rightarrow \boxed{\frac{a}{b} > \frac{1}{\sqrt{3}}}$$

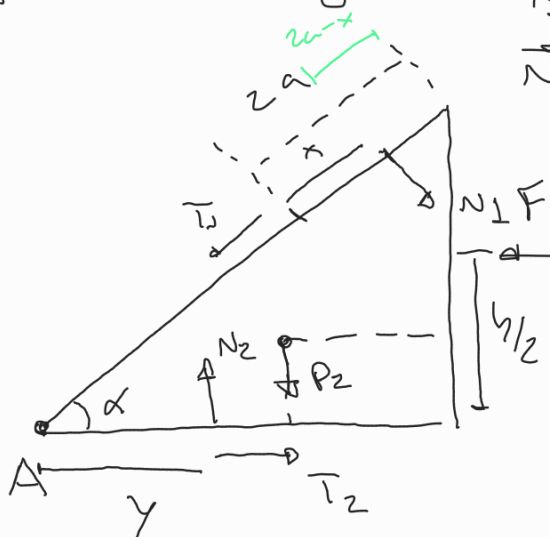
↳ $x \leq 2a$ se cumple

si no se cumple vuelva en sentido antihorario

Equilibrio triángulo

$$\vec{T}_{\perp} = T_{\perp} \cos \alpha \hat{c} + T_{\perp} \sin \alpha \hat{j}$$

$$\vec{N}_{\perp} = -N_{\perp} \sin \alpha \hat{c} + N_{\perp} \cos \alpha \hat{j}$$



$$c) T_2 - T_{\perp} \cos \alpha + N_{\perp} \sin \alpha - F = 0$$

$$j) N_2 - Mg - T_{\perp} \sin \alpha - N_{\perp} \cos \alpha = 0$$

$$\boxed{N_{\perp} = \frac{\sqrt{3}}{2} mg} \quad \left| \quad \boxed{T_{\perp} = \frac{1}{2} mg} \right.$$

$$T_2 - \frac{1}{2} \frac{\sqrt{3}}{2} mg + \frac{\sqrt{3}}{2} \frac{1}{2} mg - F = 0 \quad \boxed{F = T_2}$$

$$N_2 - Mg - \frac{1}{2} \frac{1}{2} mg - \frac{\sqrt{3}}{2} \frac{\sqrt{3}}{2} mg = 0 \quad \boxed{N_2 = (M+m)g}$$

$N_2 > 0$ se cumple \rightarrow

$$|\vec{T}_2| \leq f_E |\vec{N}_1| \rightarrow F \leq f_E (M+m)g$$

$$\tan \alpha = \frac{h}{L}$$

$$h = \frac{L}{\sqrt{3}}$$

$$\vec{M}_A^{\text{ext}} = 0 = N_2 y - Mg \frac{2L}{3} - N_1 \left(\frac{L}{\cos \alpha} - (2a-x) \right) + \frac{h}{2} F = 0$$

$$= (M+m)gy - Mg \frac{2L}{3} - \frac{\sqrt{3}}{2} mg \left(\frac{2L}{\sqrt{3}} - 2a + a - \frac{b}{\sqrt{3}} \right) + \frac{L}{2\sqrt{3}} F = 0$$

$$= (M+m)gy - Mg \frac{2L}{3} - \frac{\sqrt{3}}{2} mg \left(\frac{2L}{\sqrt{3}} - a - \frac{b}{\sqrt{3}} \right) + \frac{L}{2\sqrt{3}} F = 0$$

$$y = \frac{1}{M+m} \left[\frac{2}{3} M L + \frac{\sqrt{3}}{2} m \left(\frac{2L}{\sqrt{3}} - a - \frac{b}{\sqrt{3}} \right) - \frac{L}{2\sqrt{3}} \frac{F}{g} \right]$$

$$y = \frac{1}{M+m} \left[L \left(\frac{2}{3} M + m \right) - \frac{\sqrt{3}}{2} \left(a + \frac{b}{\sqrt{3}} \right) m - \frac{L}{2\sqrt{3}} \frac{F}{g} \right]$$

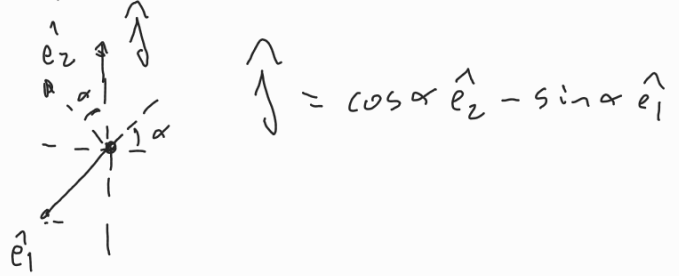
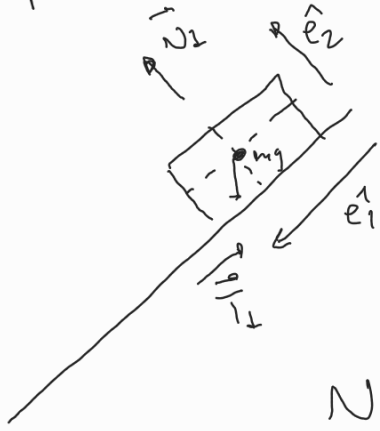
$$y = L \underbrace{\left(\frac{\frac{2}{3} M + m}{M+m} \right)}_{\uparrow} - \frac{\sqrt{3}}{2} \frac{m}{M+m} \underbrace{\left(a + \frac{b}{\sqrt{3}} \right)}_{\uparrow} - \frac{L}{2\sqrt{3}} \frac{F}{\underbrace{(M+m)g}_{\uparrow f_E}}$$

2a
pues $\frac{b}{\sqrt{3}} < a$

$0 < y < L \rightarrow y < L$ se cumple

$$0 < L \left(\frac{\frac{2}{3} M + m}{M+m} \right) - \frac{\sqrt{3}}{2} \frac{m}{M+m} \left(a + \frac{b}{\sqrt{3}} \right) - \frac{L}{2\sqrt{3}} \frac{F}{(M+m)g}$$

b) La placa triangular en equilibrio, la rectangular desliza



$$N_{\perp} - mg \cos \alpha = 0 \quad N_{\perp} = \frac{\sqrt{3}}{2} mg$$

$$mg \sin \alpha - T_{\perp} = m \ddot{x}$$

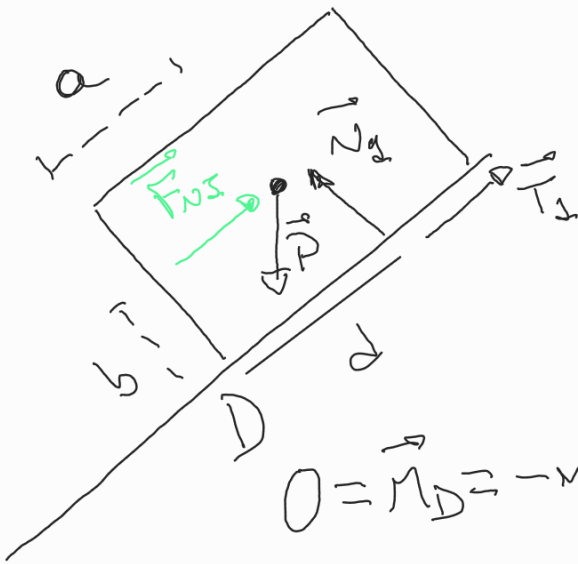
$$|\vec{T}_{\perp}| = f_D |\vec{N}_{\perp}| \Rightarrow T_{\perp} = f_D mg \cos \alpha \Rightarrow \ddot{x} = g (\sin \alpha - f_D \cos \alpha)$$

$$\ddot{x} = \frac{g}{2} (1 - \sqrt{3} f_D)$$

Observación:

$$\text{si } f_D < f_E < \frac{1}{\sqrt{3}}$$

$$\Rightarrow \ddot{x} > 0$$



$$F_{N3} = -m \ddot{x} \hat{e}_1$$

$$0 = \vec{M}_D = -m \ddot{x} b \hat{k} - mg \cos \alpha a \hat{k} + mg \sin \alpha b \hat{k} + N_D d \hat{k}$$

$$0 = -\frac{mg}{2} (1 - \sqrt{3} f_D) b + mg (b \sin \alpha - a \cos \alpha) + \frac{\sqrt{3}}{2} mg d$$

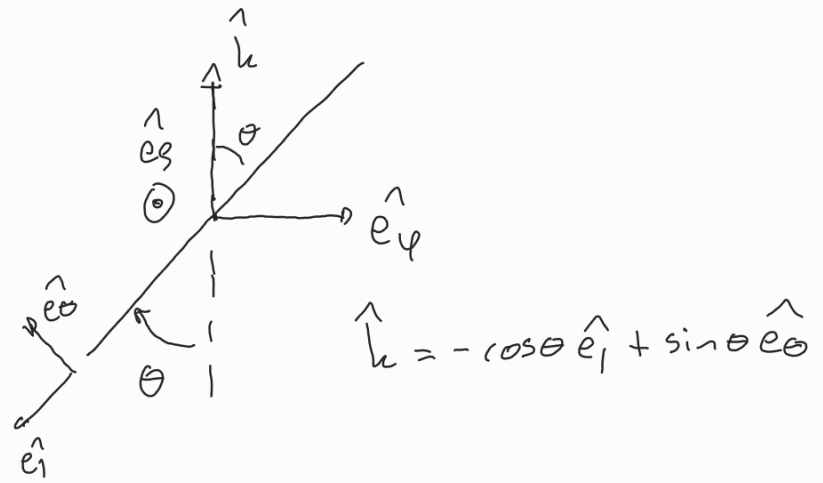
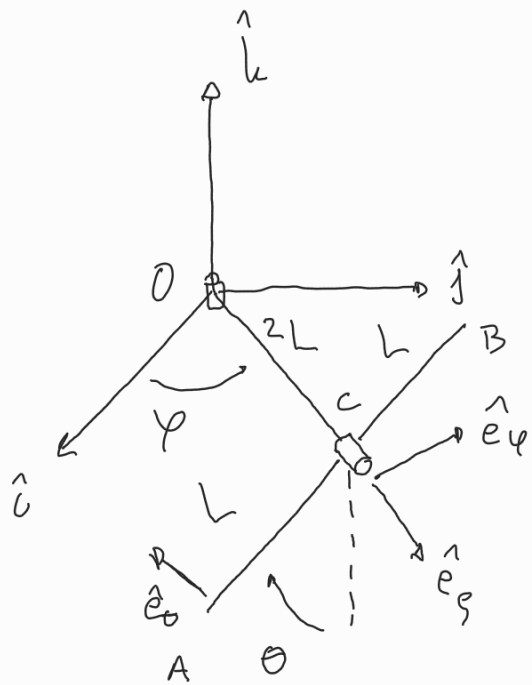
$$0 = mg \left[b \left(\frac{1}{2} - \frac{1}{2} + \frac{\sqrt{3}}{2} f_D \right) - \frac{\sqrt{3}}{2} a + \frac{\sqrt{3}}{2} d \right]$$

$$0 = \frac{\sqrt{3}}{2} mg [d + f_D b - a] \quad d = a - f_D b$$

$$0 < d < 2a \Rightarrow 0 < d \Leftrightarrow a - f_D b > 0 \Rightarrow \left[\frac{a}{b} > f_D \right]$$

$\hookrightarrow d < 2a$ se verifica.

3



a) $\vec{L}_O \cdot \hat{k}$ magnitud conservada $\Rightarrow \frac{d(\vec{L}_O \cdot \hat{k})}{dt} = 0$

$$\frac{d(\vec{L}_O \cdot \hat{k})}{dt} = \frac{d\vec{L}_O}{dt} \cdot \hat{k} + \vec{L}_O \cdot \frac{d\hat{k}}{dt}$$

$$\Rightarrow \frac{d(\vec{L}_O \cdot \hat{k})}{dt} = 0 \Rightarrow \frac{d\vec{L}_O}{dt} \cdot \hat{k} = 0$$

$$\vec{M}_O^{ext} \cdot \hat{k} = 0$$

$$\vec{M}_O^{ext} = \vec{M}_O^{react} + \vec{M}_O^{Act.}; \vec{M}_O^{react} \cdot \hat{k} = 0 \text{ por articulación cilíndrica en } O$$

$$\vec{M}_O^{Act.} = 2L \hat{e}_\varphi \wedge (-mg \hat{k}) = 2mgL \hat{e}_\varphi$$

$$\hat{e}_\varphi \cdot \hat{k} = 0$$

$$\Rightarrow \vec{M}_O^{ext} \cdot \hat{k} = 0$$

$\hookrightarrow \vec{L}_O \cdot \hat{k}$ magnitud conservada.

b) Sobre el sistema tenemos: - El peso conservativo

- Reactivas en O que son de potencia nula

- Rotaciones lisas para los ejes x y z

La energía se conserva.

$U_g = 0$ pues el centro de masa en C no cambia su altura.

c) ¿ $\vec{L}_O \cdot \hat{k}$? $\vec{L}_O = \mathbb{I}_O \vec{\omega}$

$$\vec{\omega} = \dot{\psi} \hat{k} - \dot{\theta} \hat{e}_3 \quad \vec{\omega} = -\dot{\psi} \cos \theta \hat{e}_1 + \dot{\psi} \sin \theta \hat{e}_2 - \dot{\theta} \hat{e}_3$$

$$\hat{k} = -\cos \theta \hat{e}_1 + \sin \theta \hat{e}_2$$

$$\mathbb{I}_O \{ \hat{e}_1, \hat{e}_2, \hat{e}_3 \} = \mathbb{I}_C \{ \hat{e}_1, \hat{e}_2, \hat{e}_3 \} + \mathbb{J}_O^{M,C}$$

$$\vec{r}_C - \vec{r}_O = 2L \hat{e}_3 \Rightarrow \mathbb{J}_O^{M,C} = M(2L)^2 \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix} \text{ en } \hat{e}_1, \hat{e}_2, \hat{e}_3$$

$$\mathbb{I}_C \{ \hat{e}_1, \hat{e}_2, \hat{e}_3 \} = \frac{ML^2}{12} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\mathbb{I}_O = ML^2 \begin{pmatrix} 4 & & \\ & \frac{1}{3} + 4 & \\ & & \frac{1}{3} \end{pmatrix} = \frac{ML^2}{3} \begin{pmatrix} 12 & 0 & 0 \\ 0 & 13 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\vec{L}_O = \frac{ML^2}{3} \begin{pmatrix} 12 & 0 & 0 \\ 0 & 13 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} -\dot{\psi} \cos \theta \\ \dot{\psi} \sin \theta \\ -\dot{\theta} \end{pmatrix} = \frac{ML^2}{3} \left(-12 \dot{\psi} \cos \theta \hat{e}_1 + 13 \dot{\psi} \sin \theta \hat{e}_2 - \dot{\theta} \hat{e}_3 \right)$$

$$\vec{L}_O \cdot \hat{k} = \vec{L}_O \cdot (-\cos \theta \hat{e}_1 + \sin \theta \hat{e}_2) = \frac{ML^2}{3} (12 \dot{\psi} \cos^2 \theta + 13 \dot{\psi} \sin^2 \theta)$$

$$\vec{L}_O \cdot \hat{k} = \frac{ML^2}{3} (12 + \sin^2 \theta) \dot{\varphi}$$

$$d) \quad \dot{\varphi}(0) = \dot{\varphi}_0 \quad \dot{\theta}(0) = \dot{\theta}_0 \approx 0 \quad \varphi(0) = \theta(0) = 0$$

$$T = \frac{1}{2} \vec{\omega} \cdot \mathbb{I}_O \vec{\omega}$$

$$T = \frac{1}{2} \left(-\dot{\varphi} \cos \theta \hat{e}_1 + \dot{\varphi} \sin \theta \hat{e}_2 - \dot{\theta} \hat{e}_3 \right) \cdot \frac{ML^2}{3} \left(-12 \dot{\varphi} \cos \theta \hat{e}_1 + 12 \dot{\varphi} \sin \theta \hat{e}_2 - \dot{\theta} \hat{e}_3 \right)$$

$$T = \frac{1}{2} \frac{ML^2}{3} \left(12 \dot{\varphi}^2 \cos^2 \theta + 12 \dot{\varphi}^2 \sin^2 \theta + \dot{\theta}^2 \right)$$

$$T = \frac{ML^2}{6} \left([12 + \sin^2 \theta] \dot{\varphi}^2 + \dot{\theta}^2 \right)$$

$$E = T + U = T$$

↳ defino $U_g = 0$ pues el c.m. tiene altura constante

$$\vec{L}_O \cdot \hat{k} = \frac{ML^2}{12} (12 + \sin^2 \theta) \dot{\varphi} = l_0 \quad \text{por C.I. } \varphi = \theta = 0$$

$$\dot{\varphi} = \dot{\varphi}_0$$

$$l_0 = ML^2 \dot{\varphi}_0$$

$$E_0 = \frac{ML^2}{6} (12 \dot{\varphi}_0^2 + \dot{\theta}_0^2) \approx 2 ML^2 \dot{\varphi}_0^2$$

$$\dot{\varphi} = \frac{12}{ML^2} \frac{l_0}{12 + \sin^2 \theta} = \frac{12 \dot{\varphi}_0}{12 + \sin^2 \theta}$$

Sustituyo en $E = E_0$

$$\underbrace{2 ML^2 \dot{\varphi}_0^2}_{E_0} = \frac{ML^2}{6} \left([12 + \sin^2 \theta] \left(\frac{12 \dot{\varphi}_0}{12 + \sin^2 \theta} \right)^2 + \dot{\theta}^2 \right)$$

$$12 \dot{\varphi}_0^2 = \frac{(12)^2 \dot{\varphi}_0^2}{12 + \sin^2 \theta} + \dot{\theta}^2$$

$$\theta_f = \frac{\pi}{2} \Rightarrow \sin \theta_f = 1$$

$$12 \dot{\varphi}_0^2 = \frac{(12)^2 \dot{\varphi}_0^2}{13} + \dot{\theta}_f^2$$

$$12 \left(1 - \frac{12}{13} \right) \dot{\varphi}_0^2 = \dot{\theta}_f^2 \Rightarrow \boxed{\dot{\theta}_f^2 = \frac{12}{13} \dot{\varphi}_0^2}$$

$$\dot{\varphi}_f = \frac{12}{13} \dot{\varphi}_0 \Rightarrow \vec{\omega} = \frac{12}{13} \dot{\varphi}_0 \hat{k} - \sqrt{\frac{12}{13}} \dot{\varphi}_0 \hat{e}_\theta$$

$$\vec{v}_c = 2L \dot{\varphi} \hat{e}_\varphi$$

$$\vec{v}_c(t=0) = 2L \dot{\varphi}_0 \hat{e}_\varphi$$

$$\vec{v}_c(t_f) = 2L \frac{12}{13} \dot{\varphi}_0 \hat{e}_\varphi$$