

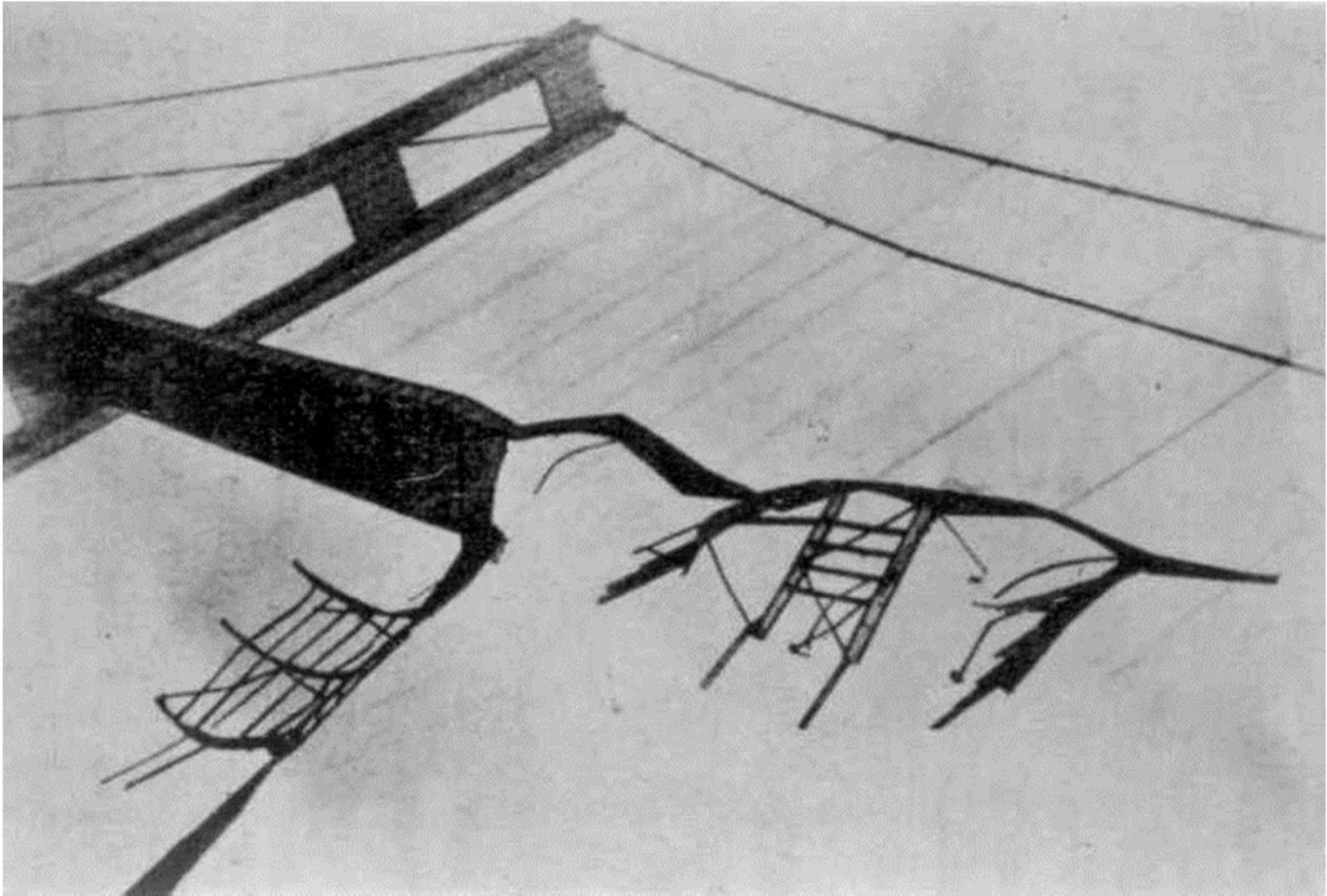
Tacoma Narrows Bridge, 1940



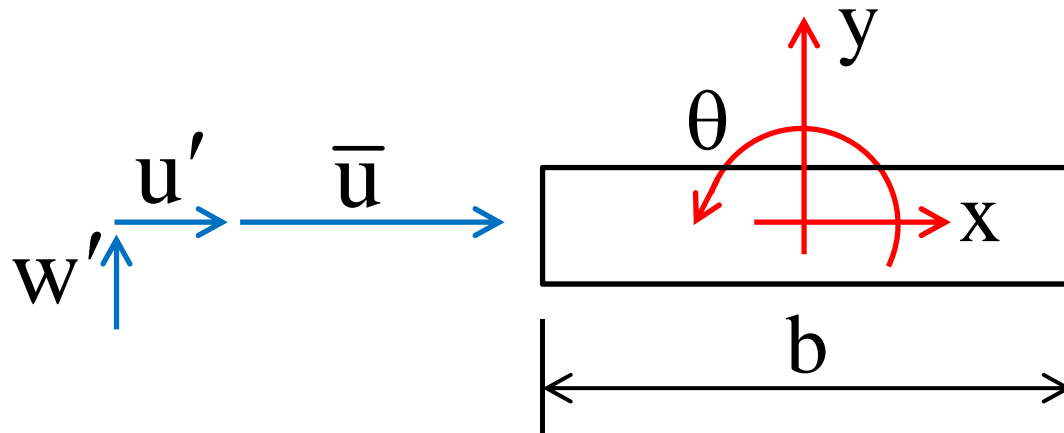
Tacoma Narrows Bridge, 1940



Tacoma Narrows Bridge, November 7, 1940



Tacoma Narrows Bridge, November 7, 1940



Simplifying hypotheses : x negligible

y and θ structurally independent

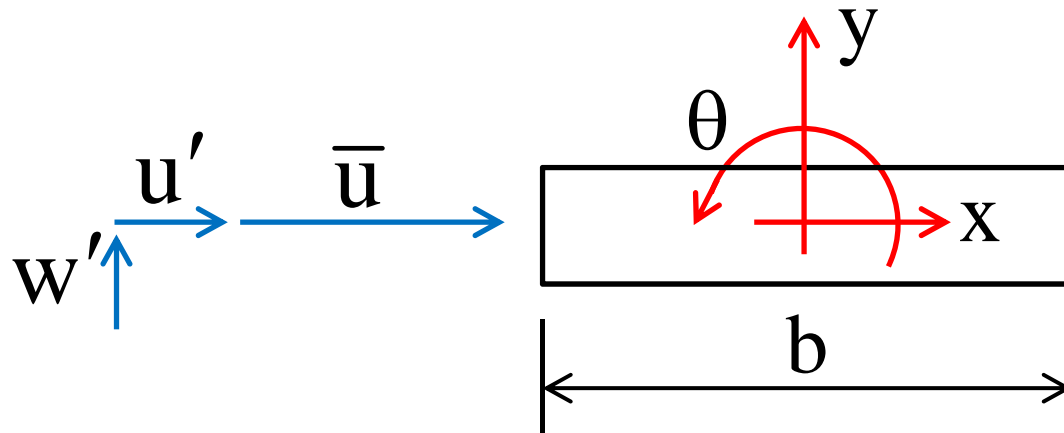
Equations of motion

$$\begin{cases} m[\ddot{y}(t) + 2\xi_y\omega_y\dot{y}(t) + \omega_y^2y(t)] = \bar{F}_y + F'_y(t) + L_a(t) \\ I[\ddot{\theta}(t) + 2\xi_\theta\omega_\theta\dot{\theta}(t) + \omega_\theta^2\theta(t)] = \bar{F}_\theta + F'_\theta(t) + M_a(t) \end{cases}$$

$\bar{F}_y, \bar{M}_\theta$ = mean wind actions

F'_y, M'_θ = fluctuating wind actions

L_a, M_a = aeroelastic (motion – induced) actions



Equations of motion

$$\begin{cases} m[\ddot{y}(t) + 2\xi_y \omega_y \dot{y}(t) + \omega_y^2 y(t)] = \bar{F}_y + F'_y(t) + L_a(t) \\ I[\ddot{\theta}(t) + 2\xi_\theta \omega_\theta \dot{\theta}(t) + \omega_\theta^2 \theta(t)] = \bar{F}_\theta + F'_\theta(t) + M_a(t) \end{cases}$$

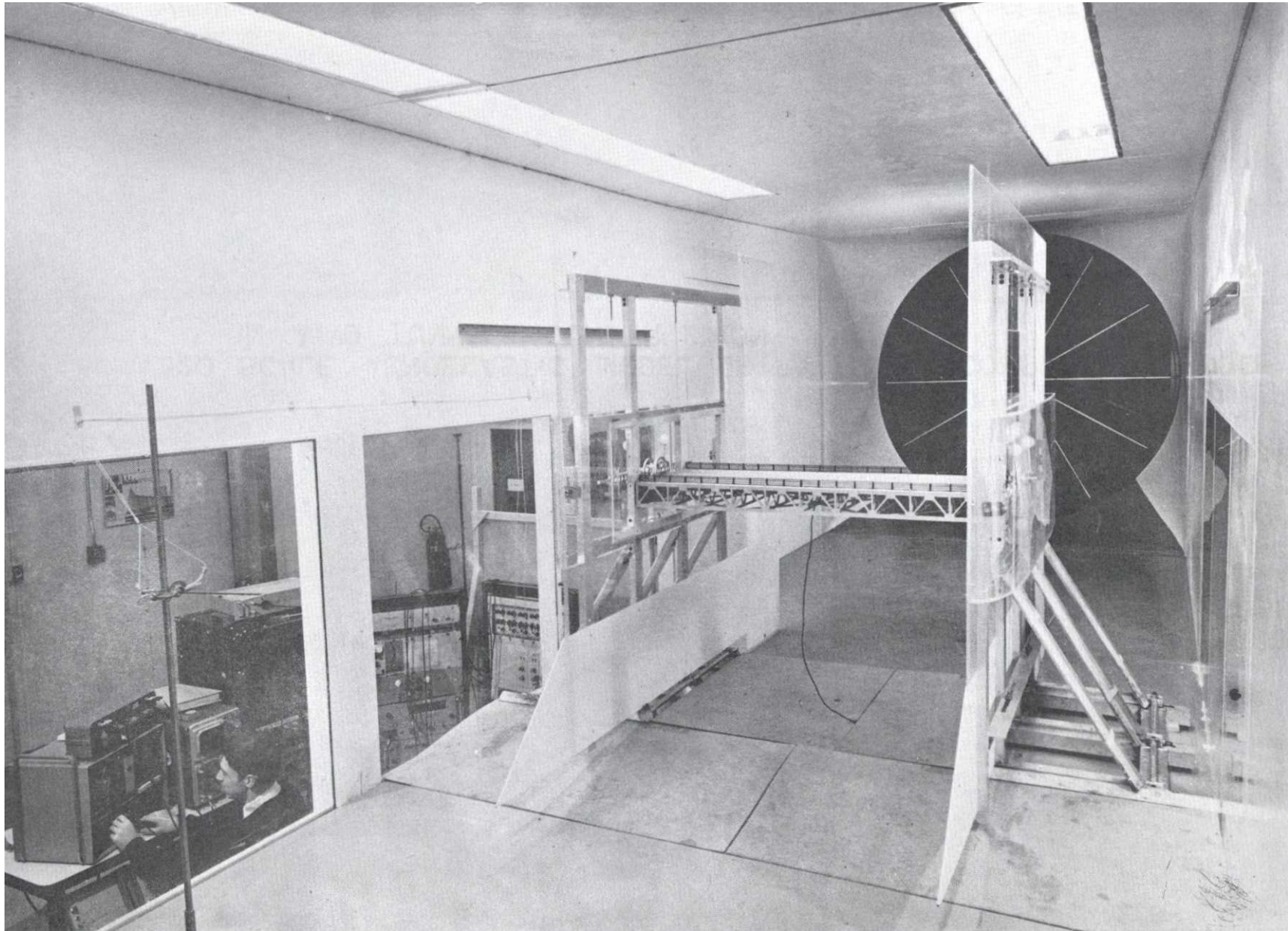
Aeroelastic actions

$$L_a(t) = \frac{1}{2} \rho \bar{u}^2 b \left[KH_1^*(K) \frac{\dot{y}(t)}{\bar{u}} + KH_2^*(K) \frac{b\dot{\theta}(t)}{\bar{u}} + K^2 H_3^*(K) \theta(t) + K^2 H_4^*(K) \frac{y(t)}{b} \right]$$

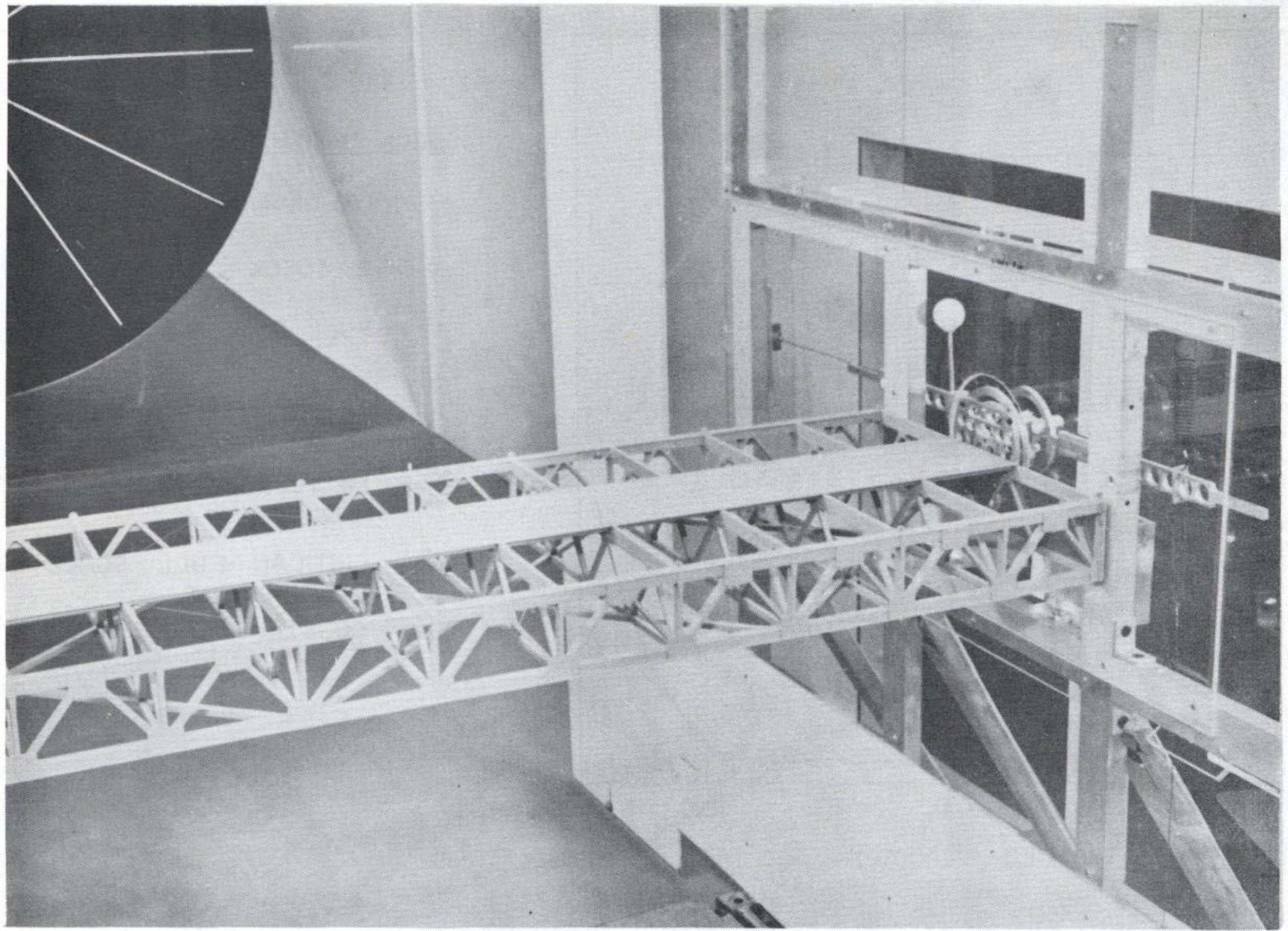
$$M_a(t) = \frac{1}{2} \rho \bar{u}^2 b^2 \left[KA_1^*(K) \frac{\dot{y}(t)}{\bar{u}} + KA_2^*(K) \frac{b\dot{\theta}(t)}{\bar{u}} + K^2 A_3^*(K) \theta(t) + K^2 A_4^*(K) \frac{y(t)}{b} \right]$$

$H_i^*(K), A_i^*(K) (i = 1, 2, 3, 4) = \text{aerodynamic derivatives}$

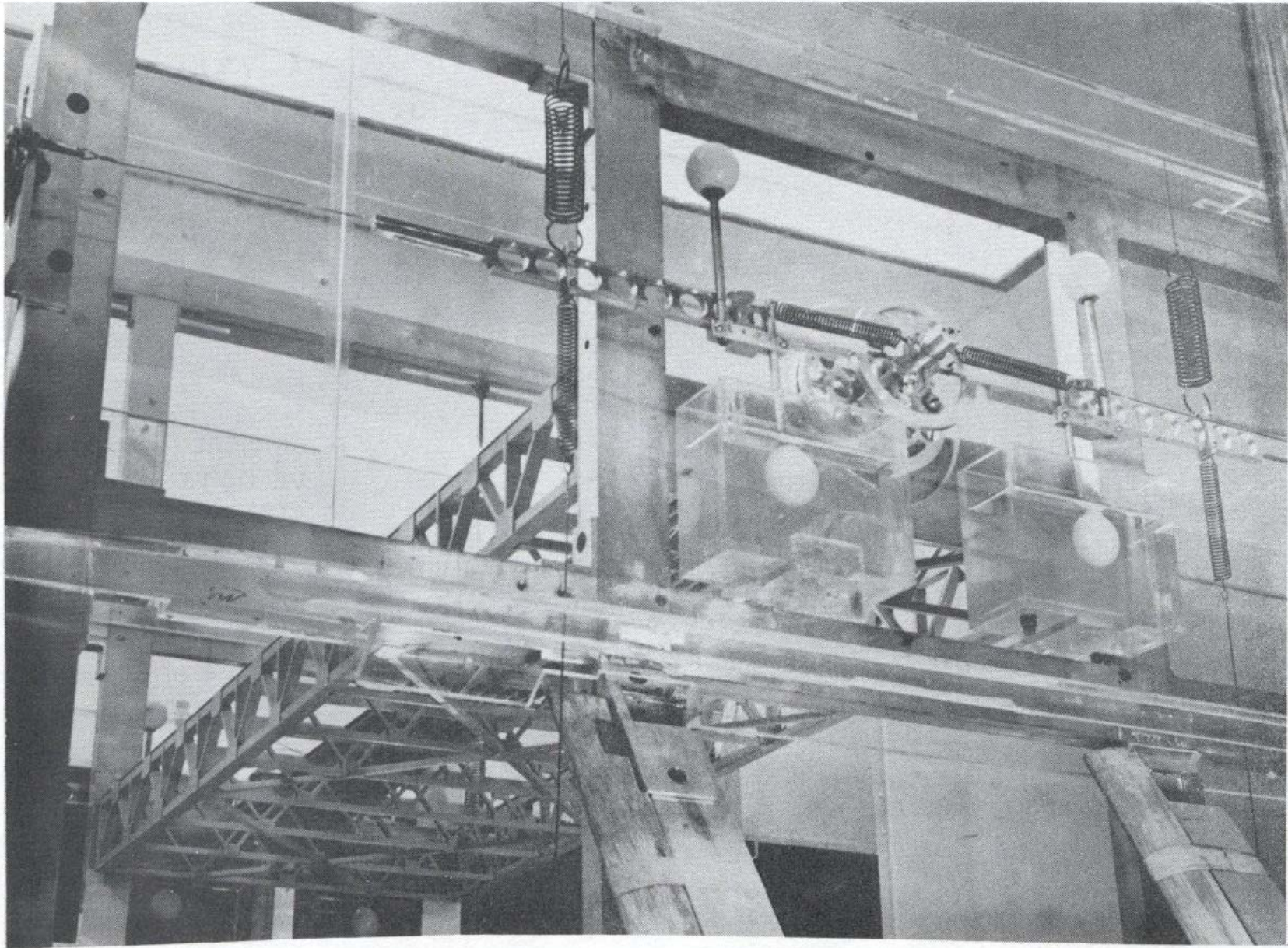
$K = \omega b / \bar{u} = \text{reduced circular frequency}$



Free-vibration wind-tunnel tests



Free-vibration wind-tunnel tests



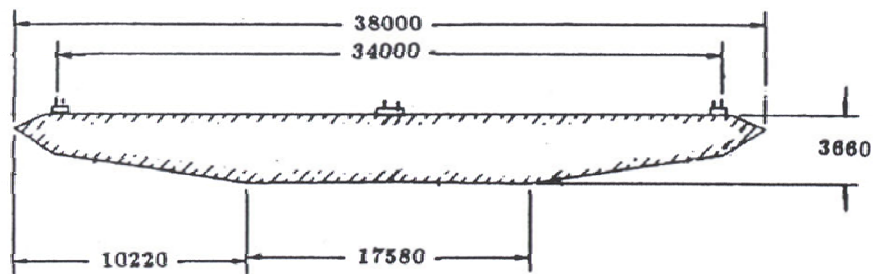
Free-vibration wind-tunnel tests



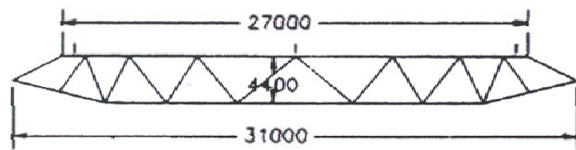
Free-vibration wind-tunnel tests



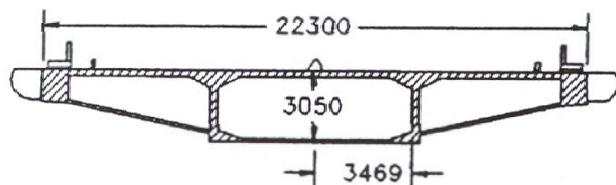
Forced-vibration wind-tunnel tests



TSURUMI FAIRWAY BRIDGE



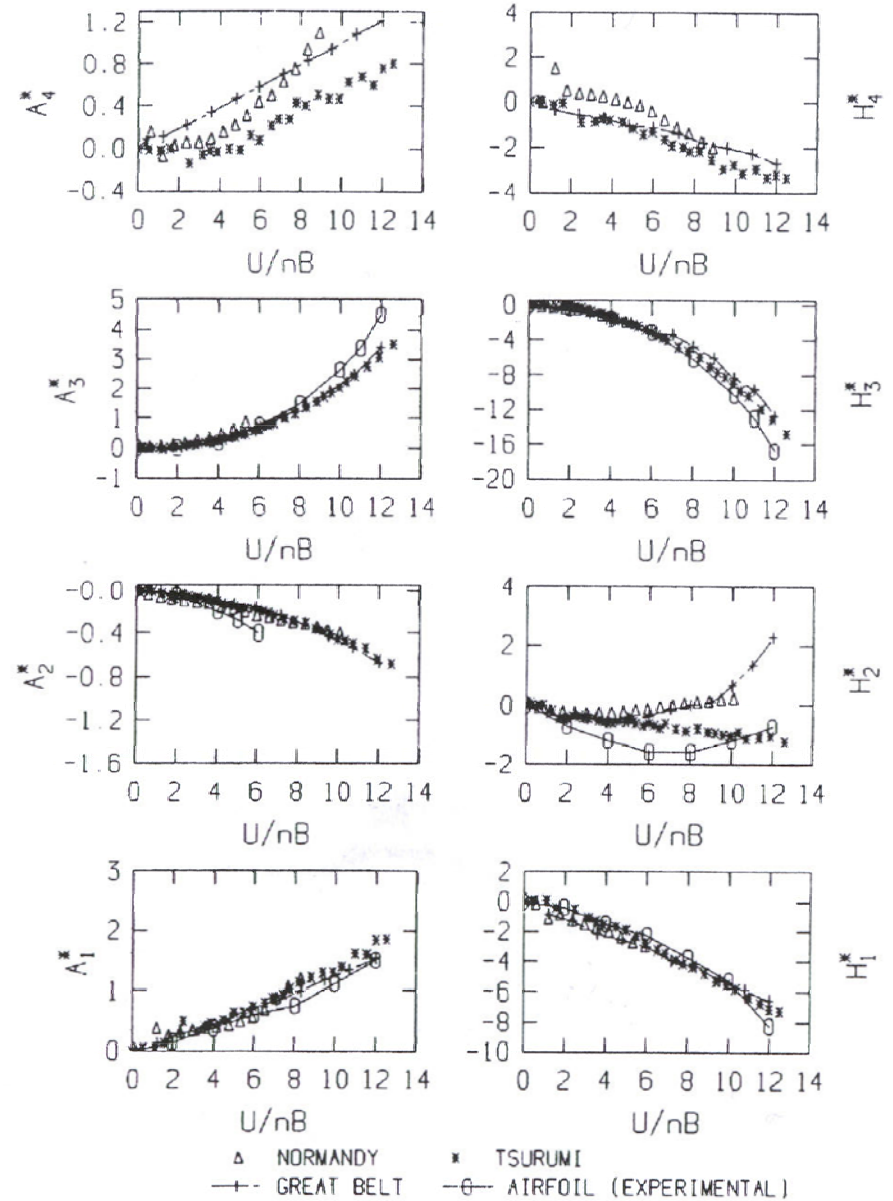
GREAT BELT EAST BRIDGE



NORMANDY BRIDGE



AIRFOIL



Aerodynamic derivatives

Equations of motion

$$\begin{cases} m \left[\ddot{y} + 2\xi_y \omega_y \dot{y} + \omega_y^2 y \right] = \bar{F}_y + F'_y + L_a \\ I \left[\ddot{\theta} + 2\xi_\theta \omega_\theta \dot{\theta} + \omega_\theta^2 \theta \right] = \bar{F}_\theta + F'_\theta + M_a \end{cases}$$

Aeroelastic actions

$$L_a = \frac{1}{2} \rho \bar{u}^2 b \left[KH_1^* \frac{\dot{y}}{\bar{u}} + KH_2^* \frac{b\dot{\theta}}{\bar{u}} + K^2 H_3^* \theta + K^2 H_4^* \frac{y}{b} \right]$$

$$M_a = \frac{1}{2} \rho \bar{u}^2 b^2 \left[KA_1^* \frac{\dot{y}}{\bar{u}} + KA_2^* \frac{b\dot{\theta}}{\bar{u}} + K^2 A_3^* \theta + K^2 A_4^* \frac{y}{b} \right]$$

Instability analysis $\Rightarrow \bar{F}_\alpha = F'_\alpha = 0 \ (\alpha = y, \theta)$

$$\begin{cases} m \left[\ddot{y} + 2\xi_y \omega_y \dot{y} + \omega_y^2 y \right] = \frac{1}{2} \rho \bar{u}^2 b \left[KH_1^* \frac{\dot{y}}{\bar{u}} + KH_2^* \frac{b\dot{\theta}}{\bar{u}} + K^2 H_3^* \theta + K^2 H_4^* \frac{y}{b} \right] \\ I \left[\ddot{\theta} + 2\xi_\theta \omega_\theta \dot{\theta} + \omega_\theta^2 \theta \right] = \frac{1}{2} \rho \bar{u}^2 b^2 \left[KA_1^* \frac{\dot{y}}{\bar{u}} + KA_2^* \frac{b\dot{\theta}}{\bar{u}} + K^2 A_3^* \theta + K^2 A_4^* \frac{y}{b} \right] \end{cases}$$

Equations of motion

$$\begin{cases} m\left[\ddot{y} + 2\xi_y\omega_y\dot{y} + \omega_y^2 y\right] = \frac{1}{2}\rho\bar{u}^2 b \left[KH_1^* \frac{\dot{y}}{\bar{u}} + KH_2^* \frac{b\dot{\theta}}{\bar{u}} + K^2 H_3^* \theta + K^2 H_4^* \frac{y}{b} \right] \\ I\left[\ddot{\theta} + 2\xi_\theta\omega_\theta\dot{\theta} + \omega_\theta^2 \theta\right] = \frac{1}{2}\rho\bar{u}^2 b^2 \left[KA_1^* \frac{\dot{y}}{\bar{u}} + KA_2^* \frac{b\dot{\theta}}{\bar{u}} + K^2 A_3^* \theta + K^2 A_4^* \frac{y}{b} \right] \end{cases}$$

$$s = \frac{\bar{u}t}{b} \Rightarrow (\cdot) = \frac{d(\cdot)}{dt} = \frac{d(\cdot)}{ds} \frac{ds}{dt} = (\cdot)' \frac{\bar{u}}{b}$$

$$K_y = \frac{\omega_y b}{\bar{u}}; K_\theta = \frac{\omega_\theta b}{\bar{u}}$$

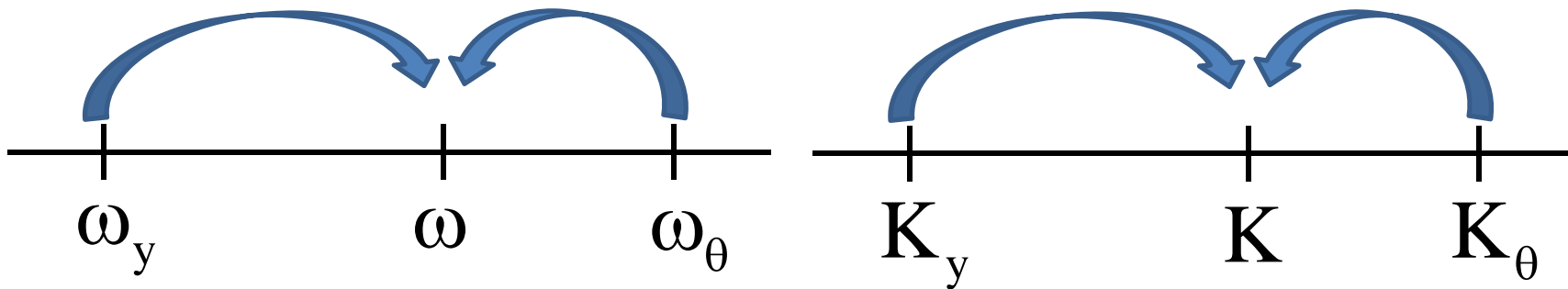
$$\begin{cases} \frac{y''}{b} + 2\xi_y K_y \frac{y'}{b} + K_y^2 \frac{y}{b} = \frac{\rho b^2}{2m} \left[KH_1^* \frac{y'}{b} + KH_2^* \theta' + K^2 H_3^* \theta + K^2 H_4^* \frac{y}{b} \right] \\ \theta'' + 2\xi_\theta K_\theta \theta' + K_\theta^2 \theta = \frac{\rho b^4}{2I} \left[KA_1^* \frac{y'}{b} + KA_2^* \theta' + K^2 A_3^* \theta + K^2 A_4^* \frac{y}{b} \right] \end{cases}$$

Equations of motion

$$\begin{cases} \frac{y''}{b} + 2\xi_y K_y \frac{y'}{b} + K_y^2 \frac{y}{b} = \frac{\rho b^2}{2m} \left[KH_1^* \frac{y'}{b} + KH_2^* \theta' + K^2 H_3^* \theta + K^2 H_4^* \frac{y}{b} \right] \\ \theta'' + 2\xi_\theta K_\theta \theta' + K_\theta^2 \theta = \frac{\rho b^4}{2I} \left[KA_1^* \frac{h'}{b} + KA_2^* \theta' + K^2 A_3^* \theta + K^2 A_4^* \frac{y}{b} \right] \end{cases}$$

$$y(t) = y_0 e^{i\omega t} ; \theta(t) = \theta_0 e^{i\omega t}$$

$$\frac{y(s)}{b} = \frac{y_0}{b} e^{iKs} ; \theta(s) = \theta_0 e^{iKs}$$



$$y(s) = y_0 e^{iKs} ; \theta(s) = \theta_0 e^{iKs}$$

Equations of motion

$$\begin{cases} \left[-K^2 + 2i\xi_y K_y K + K_y^2 - \frac{\rho b^2}{2m} (iK^2 H_1^* + K^2 H_4^*) \right] \frac{y_0}{b} - \left[\frac{\rho b^2}{2m} (iK^2 H_2^* + K^2 H_3^*) \right] \theta_0 = 0 \\ \left[-\frac{\rho b^4}{2I} (iK^2 A_1^* + K^2 A_4^*) \right] \frac{y_0}{b} + \left[-K^2 + 2i\xi_\theta K K_\theta + K_\theta^2 - \frac{\rho b^4}{2I} (iK^2 A_2^* + K^2 A_3^*) \right] \theta_0 = 0 \end{cases}$$

$$\frac{y_0}{b} = \theta_0 = 0 \Rightarrow \text{trivial solution}$$

A non-trivial solution exist if and only if the matrix of the coefficients has determinant $\Delta = 0$

$$\begin{aligned} \Delta = & \left[-K^2 + 2i\xi_y K_y K + K_y^2 - \frac{\rho b^2}{2m} (iK^2 H_1^* + K^2 H_4^*) \right] \cdot \\ & \left[-K^2 + 2i\xi_\theta K K_\theta + K_\theta^2 - \frac{\rho b^4}{2I} (iK^2 A_2^* + K^2 A_3^*) \right] + \\ & + \left[-\frac{\rho b^4}{2I} (iK^2 A_1^* + K^2 A_4^*) \right] \left[-\frac{\rho b^2}{2m} (iK^2 H_2^* + K^2 H_3^*) \right] = 0 \end{aligned}$$

$$\begin{aligned}
\Delta = & \left[-K^2 + 2i\xi_y K_y K + K_y^2 - \frac{\rho b^2}{2m} (iK^2 H_1^* + K^2 H_4^*) \right] \cdot \\
& \cdot \left[-K^2 + 2i\xi_\theta K K_\theta + K_\theta^2 - \frac{\rho b^4}{2I} (iK^2 A_2^* + K^2 A_3^*) \right] + \\
& + \left[-\frac{\rho b^4}{2I} (iK^2 A_1^* + K^2 A_4^*) \right] \left[-\frac{\rho b^2}{2m} (iK^2 H_2^* + K^2 H_3^*) \right] = 0
\end{aligned}$$

$$X = \frac{K}{K_y} = \frac{\omega}{\omega_y} \Rightarrow$$

$$\begin{aligned}
\Delta = & \left[-X^2 + 2i\xi_y X + 1 - \frac{\rho b^2}{2m} (iX^2 H_1^* + X^2 H_4^*) \right] \cdot \\
& \cdot \left[-X^2 + 2i\xi_\theta X \frac{\omega_\theta}{\omega_y} + \left(\frac{\omega_\theta}{\omega_y} \right)^2 - \frac{\rho b^4}{2I} (iX^2 A_1^* + iX^2 A_3^*) \right] + \\
& + \left[-\frac{\rho b^4}{2I} (iX^2 A_1^* + X^2 A_4^*) \right] \left[\frac{\rho b^2}{2m} (iX^2 H_2^* + X^2 H_3^*) \right] = 0
\end{aligned}$$

$$\Delta = \left[-X^2 + 2i\xi_y X + 1 - \frac{\rho b^2}{2m} (iX^2 H_1^* + X^2 H_4^*) \right] \cdot \left[-X^2 + 2i\xi_\theta X \frac{\omega_\theta}{\omega_y} + \left(\frac{\omega_\theta}{\omega_y} \right)^2 - \frac{\rho b^4}{2I} (iX^2 A_1^* + iX^2 A_3^*) \right] + \left[-\frac{\rho b^4}{2I} (iX^2 A_1^* + X^2 A_4^*) \right] \left[\frac{\rho b^2}{2m} (iX^2 H_2^* + X^2 H_3^*) \right] = 0 \Rightarrow$$

Complex equation of the 4th degree in the complex unknown X

$$a_4(K)X^4 + a_3(K)X^3 + a_2(K)X^2 + a_1(K)X + a_0(K) = 0$$

$$X = \frac{\omega}{\omega_y} = X_r + iX_i \Rightarrow \omega = \omega_r + i\omega_i \Rightarrow$$

$$\begin{cases} y(t) = y_0 e^{i\omega t} = y_0 e^{i\omega_r t} e^{-\omega_i t} \\ \theta(t) = \theta_0 e^{i\omega t} = \theta_0 e^{i\omega_r t} e^{-\omega_i t} \end{cases}$$

$\omega_i > 0 \Rightarrow$ asymptotically stable system

$\omega_i = 0 \Rightarrow$ stable system

$\omega_i < 0 \Rightarrow$ unstable system

$\omega_i = 0 \Rightarrow$ bifurcation condition \Rightarrow flutter occurrence $\Rightarrow \omega = \omega_r$

Complex equation of the 4th degree in the complex unknown X as a function of K

$$a_4(K)X^4 + a_3(K)X^3 + a_2(K)X^2 + a_1(K)X + a_0(K) = 0$$

Search for the solution of the complex equation of the 4th degree under the condition that the unknown X is real

$$\left[b_4(K)X^4 + b_3(K)X^3 + b_2(K)X^2 + b_1(K)X + b_0(K) \right] + \\ + i \left[c_4(K)X^4 + c_3(K)X^3 + c_2(K)X^2 + c_1(K)X + c_0(K) \right] = 0 \Rightarrow$$

Two real equations of the 4th degree in the real unknown X as a function of K

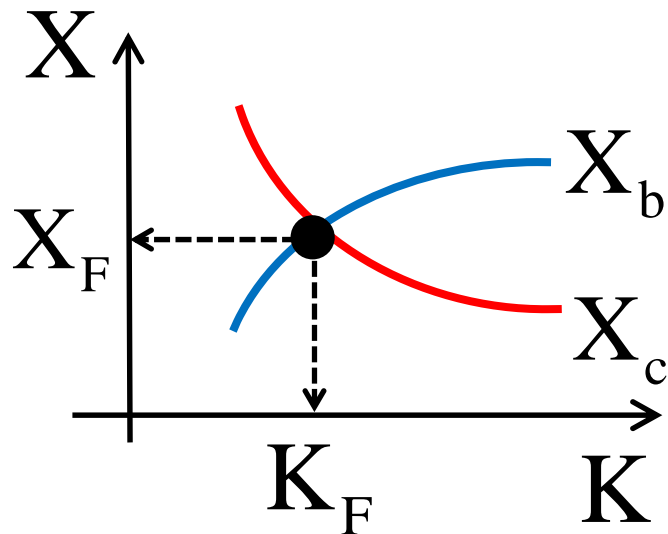
$$\begin{cases} b_4(K)X^4 + b_3(K)X^3 + b_2(K)X^2 + b_1(K)X + b_0(K) = 0 \\ c_4(K)X^4 + c_3(K)X^3 + c_2(K)X^2 + c_1(K)X + c_0(K) = 0 \end{cases}$$

Two real equations of the 4th degree in the real unknown X as a function of K

$$\begin{cases} b_4(K)X^4 + b_3(K)X^3 + b_2(K)X^2 + b_1(K)X + b_0(K) = 0 \\ c_4(K)X^4 + c_3(K)X^3 + c_2(K)X^2 + c_1(K)X + c_0(K) = 0 \end{cases}$$

Complex and negative solutions are disregarded \Rightarrow

$$X_b = X_b(K); X_c = X_c(K)$$



Flutter circular frequency

$$\omega_F = \omega_y X_F$$

Flutter critical velocity

$$\bar{u}_F = \frac{\omega_F b}{K_F}$$

CLASSICAL FLUTTER

2 D.O.F. coupled vertical and torsional flutter

$$\begin{cases} m\left[\ddot{y} + 2\xi_y\omega_y\dot{y} + \omega_y^2y\right] = \frac{1}{2}\rho\bar{u}^2b\left[KH_1^*\frac{\dot{y}}{\bar{u}} + KH_2^*\frac{b\dot{\theta}}{\bar{u}} + K^2H_3^*\theta + K^2H_4^*\frac{y}{b}\right] \\ I\left[\ddot{\theta} + 2\xi_\theta\omega_\theta\dot{\theta} + \omega_\theta^2\theta\right] = \frac{1}{2}\rho\bar{u}^2b^2\left[KA_1^*\frac{\dot{y}}{\bar{u}} + KA_2^*\frac{b\dot{\theta}}{\bar{u}} + K^2A_3^*\theta + K^2A_4^*\frac{y}{b}\right] \end{cases}$$

STALL FLUTTER

1 D.O.F. torsional flutter

$$I\left[\ddot{\theta} + 2\xi_\theta\omega_\theta\dot{\theta} + \omega_\theta^2\theta\right] = \frac{1}{2}\rho\bar{u}^2b^2KA_2^*\frac{b\dot{\theta}}{\bar{u}} \Rightarrow$$

$$\ddot{\theta} + 2\left[\xi_\theta - \frac{\rho b^4}{4I} \frac{\omega}{\omega_\theta} A_2^*\right]\omega_\theta\dot{\theta} + \omega_\theta^2\theta = 0$$

STALL FLUTTER – 1 D.O.F. torsional flutter

$$\ddot{\theta} + 2 \left[\xi_{\theta} - \frac{\rho b^4}{4I} \frac{\omega}{\omega_{\theta}} A_2^* \right] \omega_{\theta} \dot{\theta} + \omega_{\theta}^2 \theta = 0$$

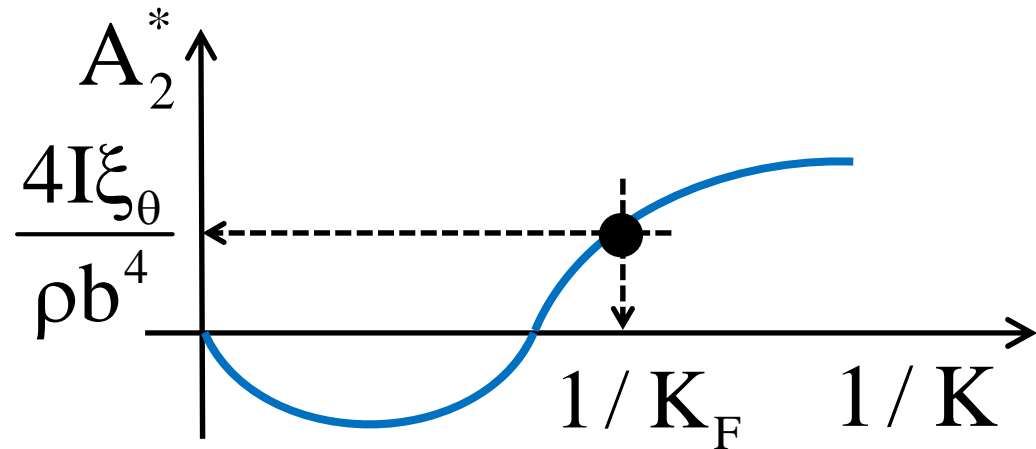
Flutter critical condition

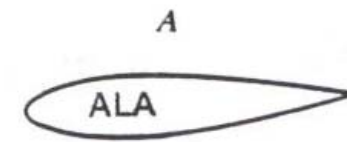
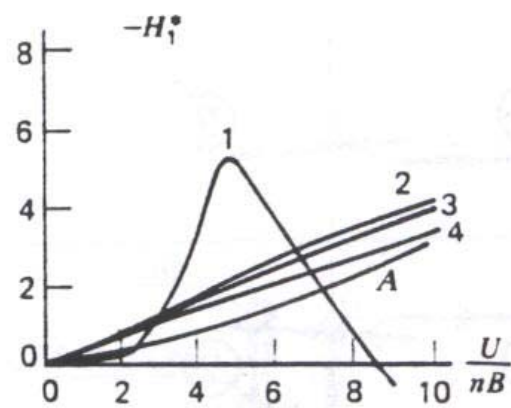
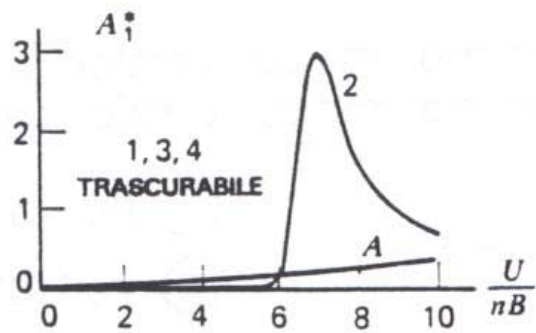
$$\omega = \omega_{\theta}$$

$$A_2^* = \frac{4I\xi_{\theta}}{\rho b^4}$$

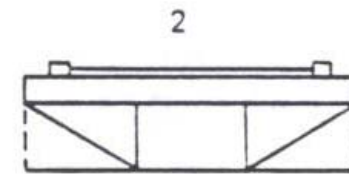
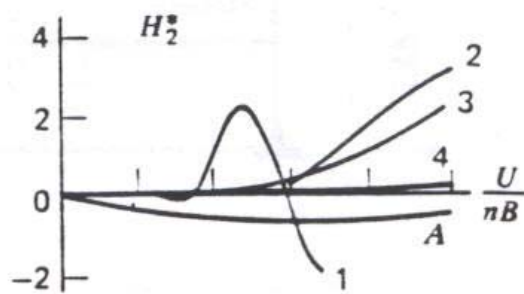
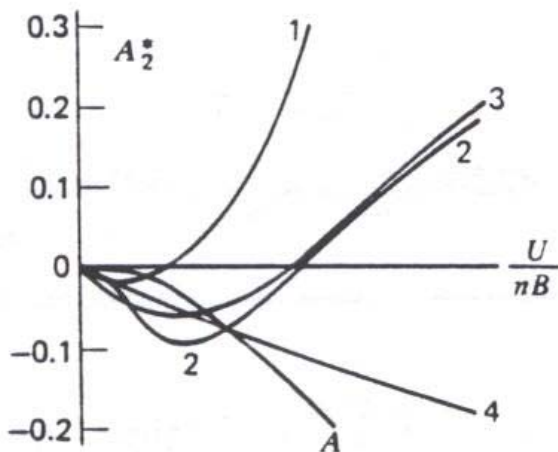
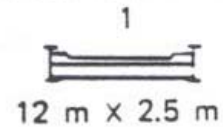
Flutter critical velocity

$$\bar{u}_F = \frac{b\omega_{\theta}}{K_F}$$

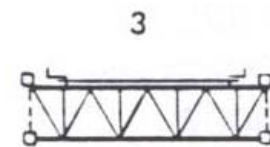




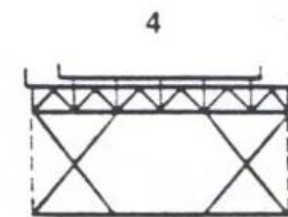
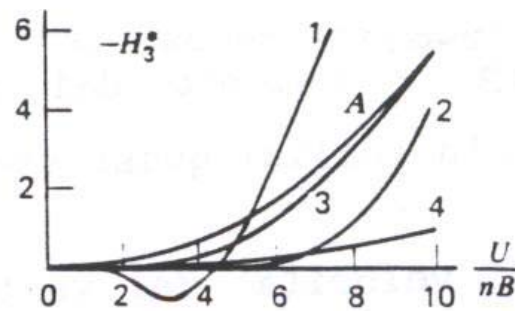
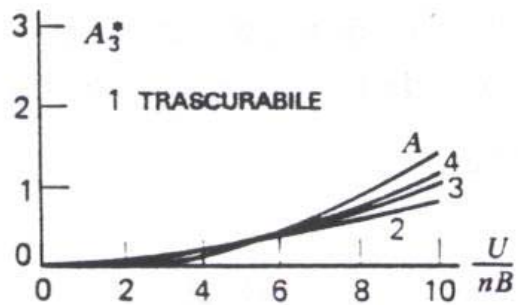
PONTE "ORIGINAL TACOMA NARROWS"



27.5 m x 7.5 m



20 m x 5 m

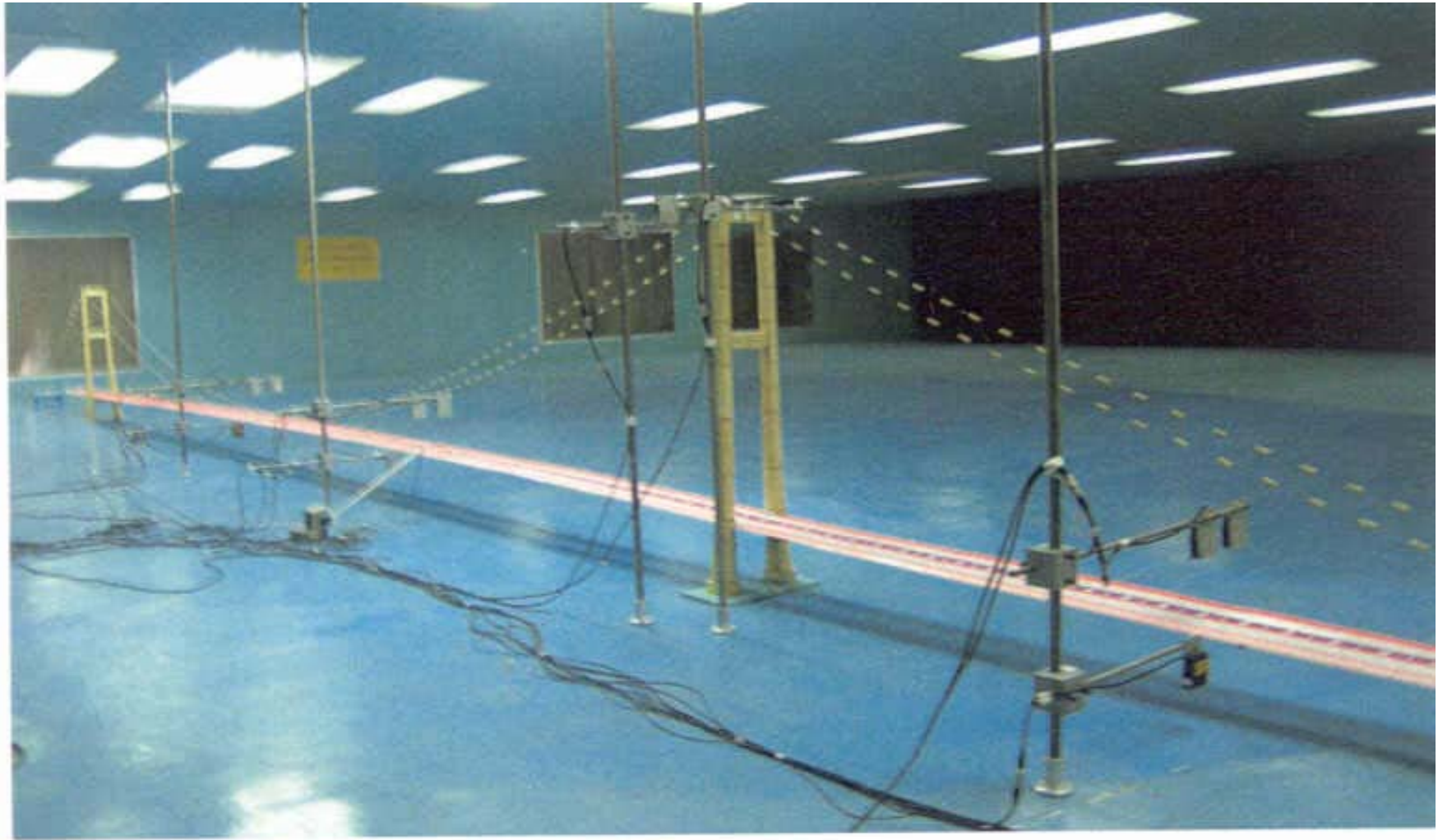


21.5 m x 10.5 m

Flutter derivatives



Great Belt East Bridge, 1997



Xihoumen Bridge, China, 2008



Akashi-Kaikyo Bridge, 1998



Akashi-Kaikyo Bridge, 1998



Akashi-Kaikyo Bridge, 1998